

# IRRIGATION MANAGEMENT GUIDELINES FOR CITRUS AND ALFALFA BASINS IN THE YUMA MESA IRRIGATION DISTRICT: MANUAL OF PRACTICE

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Final project report

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Water measuring flume installed in the field water supply channel of a grower's farm to help raise irrigation application efficiency



Portable flumes installed in farm water supply channels provides irrigators with a capability to better control the water supply to their irrigation basins



Improved accuracy in water measurement and control allows accurate quantification of irrigation efficiency and deep percolation losses

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## MANAGEMENT GUIDELINE

The following is a step by step guideline for making improved management decisions for citrus and alfalfa basins in the Yuma Mesa using the modified management tables (Tables 2a-4k) and the associated correction procedure presented in project report:

1. Select alternative unit inlet flow rate ( $q_o$ ) and cutoff time ( $t_{co}$ ) combinations from the management tables (Table 2a-4k).
2. For each alternative management scenario, determine the appropriate correction factors,  $C_{fa}$ , using the associated cutoff distances from Tables 2a-4k and Table 1. Then, calculate the corrected cutoff times ( $t_{coC}$ ) for each management option as follows:

$$t_{coC} = (1 + C_{fa})t_{co} \quad (5)$$

Where  $C_{fa}$  = the advance time correction factor (Table 1).

3. For each alternative scenario, calculate the total time required to irrigate all basins in the farm without accounting for down-time ( $t_{ai}$ ) and the inflow into a basin ( $Q$ ):

$$t_{ai} = N_b t_{coC} \quad \text{and} \quad Q = q_o W_b \quad (6)$$

where  $N_b$  = number of basins in a block that are to be irrigated in a single irrigation session.

4. For each combination of  $Q$  and  $t_{ai}$ , determine the total duration of water supply from the main canal after allowing for downtime ( $t_i$ ).

$$t_i = (1 + C_{fi})t_{ai} \quad (7)$$

where  $C_{ft}$  = a factor that represents a fraction of  $t_i$  that is used as downtime to fill the field supply channel and to account for accidental leaks and seepage.  $C_{ft}$  can be calculated as

$$C_{ft} = \frac{(zy^2 + by)L_c}{t_{ai}Q} + 0.05 \quad (8)$$

where the first term on the right hand side represents the contribution of the volume of water retained in the field supply channel, the constant (0.05) accounts for water lost due leakage and seepage,  $z$  = side slope of field supply channel (horizontal/vertical) [-],  $y$  = flow depth [ft],  $b$  = channel bottom width [ft], and  $L_c$  = channel length [ft].

5. Summarize the alternative management scenarios and select the irrigation scenario with the highest application efficiency. *Caution:* It is tempting to choose a scenario that combines smaller inlet inflow rates with shorter cutoff times, as these scenarios often result in apparently higher application efficiencies. It is, however, important to note that these irrigation scenarios are likely to result in infeasible irrigations.

*An example problem for level basin management*

Given:

A grower has 15 irrigation basins to irrigate his citrus grove located in the Yuma Mesa. Each basin in the farm is 600 ft long 110 ft wide. The grower agreed with the Yuma Mesa Irrigation District to have a degree of flexibility with respect to the discharge that he can withdraw from the main canal and its duration, provided the grower communicates his decision to the irrigation district a week ahead of a scheduled irrigation event. Further, all the 15 basins are to be irrigated in a single session. Each basin has two furrows that run along the edges

of the basin. Downtime can be taken as 10% of the actual time used to irrigate the basins.

Required:

To determine the inlet flow rate and cutoff time combination that yields acceptable performance.

Solution:

1. Three alternative management scenarios are considered:

Management options summary table

Option	$L_{co}$	$t_{co}$	$q_o$	$E_a$	$E_r$	$D_{ulq}$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
	ft	min	Cfs/ft	%	%	-	in	in	in	in	in
I	362.5	16	0.16	49.0	100	0.99	1.5	2.9	2.9	3.01	7.3
II	362.5	17	0.14	52.0	100	0.99	1.3	2.8	2.8	2.85	6.8
III	387.5	22	0.10	55.0	100	0.99	1.2	2.6	2.6	2.61	5.8

These values were obtained from Tables 2b, 2d, and 2g

2. Determine the  $C_{fa}$  and  $t_{coC}$  values for each management alternative. From Table 1, approximate values of  $C_{fa}$  are: for management option I,  $C_{fa} = 0.19$ ; for management option II,  $C_{fa} = 0.19$ ; and for management option III,  $C_{fa} = 0.16$ . The  $t_{coC}$  values corresponding to each management scenario is calculated using Eq. 5 and summarized below:

Management options summary table

Option	$L_{co}$	$t_{co}$	$t_{coC}$	$q_o$	$E_a$	$E_r$	$D_{ulq}$	$D_p$	$D_{app}$	$Y_{max}$
	ft	min	min	cfs/ft	%	%	-	in	in	in
I	362.5	16	19	0.16	49.0	100	0.99	1.5	3.01	7.3
II	362.5	17	21	0.14	52.0	100	0.99	1.3	2.85	6.8
III	387.5	22	26	0.10	55.0	100	0.99	1.2	2.61	5.8

Note that calculated  $t_{coC}$  values are rounded to the nearest integer.

3. For each management scenario, calculate the time required to irrigate all basins in the farm ( $t_{ai}$ ) and the inflow into a basin ( $Q$ ) using Eq. 6. The following a summary of the result:

Management options summary table

Option	$L_{co}$	$t_{co}$	$t_{coC}$	$t_{ai}$	$q_o$	$Q$	$E_a$	$E_r$	$D_{ulq}$	$D_p$	$D_{app}$	$Y_{max}$
	ft	min	min	min	cfs/ft	cfs	%	%	-	in	in	in
I	362.5	16	19	285	0.16	17.6	49.0	100	0.99	1.5	3.01	7.3
II	362.5	17	20	300	0.14	15.4	52.0	100	0.99	1.3	2.85	6.8
III	387.5	22	26	390	0.10	11.0	55.0	100	0.99	1.2	2.61	5.8

4. For each management alternative calculate the required duration of water supply from the main canal after allowing for downtime ( $t_i$ ) using Eq. 7. The  $t_i$  calculated using a safety factor of approximately 0.075-0.08 (calculated using Eq. 8 for a channel with a side slope of 1, flow depth of 1.3 ft, and bottom width of 2.3 ft) is summarized below:

Management options summary table

Option	$L_{co}$	$t_{co}$	$t_{coC}$	$t_{ai}$	$t_i$	$q_o$	$Q$	$E_a$	$E_r$	$D_{ulq}$	$D_p$	$D_{app}$	$Y_{max}$
	ft	min	min	min	min	cfs/ft	cfs	%	%	-	in	in	in
I	362.5	16	19	285	307	0.16	17.6	49.0	100	0.99	1.5	3.01	7.3
II	362.5	17	20	300	323	0.14	15.4	52.0	100	0.99	1.3	2.85	6.8
III	387.5	22	26	390	421	0.10	11.0	55.0	100	0.99	1.2	2.61	5.8

Check with the irrigation district if all the  $t_i$ - $Q$  combinations are feasible options.

5. Assuming all options are feasible, from the point of view of irrigation performance, the third option is to be selected. In which case, the grower will withdraw a discharge of 11.0 cfs from the main canal for approximately 421 min. There will be a “down-time” of 31 min. With this management scenario, the entire farm will be irrigated in about 7 hrs. The resulting performance is:  $E_a = 55\%$ ,  $E_r = 100\%$ , and  $Du_{lq} = 0.99$ .

## **SUMMARY**

A management package has been proposed for the citrus and alfalfa basins of the Yuma Mesa. While much of the development here is based on management tables reported earlier by the authors, in this study the management tables were modified and procedures were developed to bring the management tables in close agreement with field observations. In addition, management tables are compiled for three more basin lengths that are found in the Yuma Mesa (500 ft, 700 ft, and 800 ft). The procedure outlined above and in the project report is applicable to these set of management tables as well.

The management tools are based on average field conditions (infiltration, roughness, micro-topography, crop) assumed to prevail in the Yuma Mesa area. To the extent this conditions are met in the field, the tools and guidelines presented here are useful management aids. However, it is important to note that individual field conditions can differ from the conditions assumed here, therefore growers are advised to complement their decisions with their best judgment rooted in experience. Especially, growers are advised to fine tune the correction factor continuously based on actual field experience. It is important to note that periodic land leveling and calibration of the flow measuring devices are integral components of the irrigation management procedure proposed here.

Achievable performance levels shown in Tables 2a-4k are generally low. This indicates that for the field conditions in the Yuma Mesa the basin length used (600 ft) is too high. Thus, it ought to be noted that much higher level of performance can be achieved if smaller basins are to be used. The gain in performance, however, need to be carefully gauged against losses in terms of land taken out of cultivation and machinery idle runs before any such decision is made by an individual grower.

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**Table 1.** Approximate correction factors

<i>Cutoff ratio <math>L_{co}/L^1</math></i>		0.50	0.55	0.60	0.65	0.70	0.75	0.80	0.85	0.90	0.95	1.0
$C_{fa}$	<i>Level basin</i>	0.25	0.22	0.19	0.16	0.13	0.10	0.0	0.0	0.0	0.0	0.0
	<i>Graded basin</i>	0.25	0.20	0.15	0.10	0.0	0.0	0.0	0.0	0.0	0.0	0.0

<sup>1</sup> $L_{co}$  = cutoff distance obtained from tables 1a-3k,  $L$  = basin length

<b>Table 2a</b> Lookup table for level basins, <i>CITRUS</i>										
$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.04</b>	<b>362.5</b>	36	84.6	0.97	100	0.2	1.7	1.60	1.68	3.8
	<b>387.5</b>	40	77.6	0.97	100	0.4	1.8	1.75	1.85	3.8
	<b>412.5</b>	43	71.6	0.98	100	0.5	2.0	2.00	2.05	3.8
	<b>437.5</b>	46	66.5	0.98	100	0.7	2.1	2.10	2.25	3.8
	<b>462.5</b>	50	61.9	0.98	100	0.9	2.3	2.30	2.42	3.8
	<b>487.5</b>	53	57.9	0.98	100	1.0	2.4	2.50	2.51	3.8
	<b>512.5</b>	56	54.7	0.98	100	1.2	2.6	2.60	2.72	3.8
	<b>537.5</b>	60	51.5	0.98	100	1.3	2.8	2.80	2.90	3.8
	<b>562.5</b>	64	48.5	0.98	100	1.5	2.9	3.00	3.15	3.8
	<b>587.5</b>	67	45.8	0.98	100	1.7	3.1	3.20	3.23	3.8
	<b>600.0</b>	68	44.9	0.98	100	1.8	3.2	3.20	3.25	3.8
<b>0.05</b>	<b>362.5</b>	32	78.0	0.98	100	0.4	1.8	1.8	1.85	4.2
	<b>387.5</b>	34	71.6	0.98	100	0.5	2.0	2.0	2.12	4.2
	<b>412.5</b>	37	66.0	0.98	100	0.7	2.2	2.1	2.28	4.2
	<b>437.5</b>	40	61.3	0.98	100	0.9	2.4	2.3	2.45	4.2
	<b>462.5</b>	43	57.1	0.98	100	1.1	2.5	2.5	2.61	4.2
	<b>487.5</b>	46	53.4	0.98	100	1.2	2.7	2.7	2.80	4.2
	<b>512.5</b>	49	50.5	0.98	100	1.4	2.9	2.8	2.95	4.2
	<b>537.5</b>	52	47.5	0.99	100	1.6	3.1	3.0	3.14	4.2
	<b>562.5</b>	55	44.8	0.99	100	1.8	3.2	3.2	3.25	4.2
	<b>587.5</b>	58	42.4	0.99	100	2.0	3.4	3.4	3.50	4.2
	<b>600.0</b>	59	41.4	0.99	100	2.0	3.5	3.5	3.60	4.2

<sup>1</sup>values are rounded-off to the nearest integer

<b>Table 2b</b> Lookup table for level basins, <i>CITRUS</i>										
$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>Ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.06</b>	<b>362.5</b>	28	72.8	0.98	100	0.5	2.0	1.9	2.05	4.6
	<b>387.5</b>	31	66.8	0.98	100	0.7	2.2	2.1	2.25	4.6
	<b>412.5</b>	33	61.6	0.98	100	0.9	2.3	2.3	2.41	4.6
	<b>437.5</b>	36	57.2	0.98	100	1.1	2.5	2.5	2.60	4.6
	<b>462.5</b>	38	53.3	0.99	100	1.2	2.7	2.7	2.75	4.6
	<b>487.5</b>	41	49.8	0.99	100	1.4	2.9	2.9	3.00	4.6
	<b>512.5</b>	43	47.2	0.99	100	1.6	3.0	3.0	3.17	4.6
	<b>537.5</b>	46	44.3	0.99	100	1.8	3.3	3.2	3.37	4.6
	<b>562.5</b>	49	41.8	0.99	100	2.0	3.5	3.4	3.47	4.6
	<b>587.5</b>	52	39.6	0.99	100	2.2	3.7	3.6	3.77	4.6
	<b>600.0</b>	53	38.7	0.99	100	2.3	3.8	3.7	3.82	4.6
<b>0.07</b>	<b>362.5</b>	26	68.6	0.98	100	0.6	2.1	2.1	2.18	4.9
	<b>387.5</b>	28	63.0	0.98	100	0.8	2.3	2.3	2.36	4.9
	<b>412.5</b>	30	58.1	0.98	100	1.0	2.5	2.4	2.56	4.9
	<b>437.5</b>	33	53.99	0.99	100	1.2	2.7	2.6	2.76	4.9
	<b>462.5</b>	35	50.22	0.99	100	1.4	2.9	2.9	2.98	4.9
	<b>487.5</b>	37	47.00	0.99	100	1.6	3.1	3.1	3.18	4.9
	<b>512.5</b>	39	44.50	0.99	100	1.8	3.3	3.2	3.27	4.9
	<b>537.5</b>	42	41.80	0.99	100	2.0	3.5	3.4	3.47	4.9
	<b>562.5</b>	45	39.40	0.99	100	2.2	3.7	3.7	3.77	4.9
	<b>587.5</b>	47	37.30	0.99	100	2.4	3.9	3.9	3.98	4.9
	<b>600.0</b>	48	36.50	0.99	100	2.5	4.0	4.0	4.08	4.9

<sup>1</sup>values are rounded-off to the nearest integer

<b>Table 2c</b> Lookup table for level basins, <i>CITRUS</i>										
$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.08</b>	<b>362.5</b>	24	65.1	0.98	100	0.7	2.2	2.2	2.30	5.3
	<b>387.5</b>	26	59.8	0.99	100	0.9	2.4	2.4	2.50	5.3
	<b>412.5</b>	28	55.2	0.99	100	1.1	2.6	2.6	2.70	5.3
	<b>437.5</b>	30	51.2	0.99	100	1.4	2.8	2.8	2.90	5.3
	<b>462.5</b>	32	47.7	0.99	100	1.6	3.0	3.0	3.10	5.3
	<b>487.5</b>	34	44.6	0.99	100	1.8	3.3	3.2	3.16	5.3
	<b>512.5</b>	36	42.2	0.99	100	2.0	3.4	3.4	3.50	5.3
	<b>537.5</b>	39	39.7	0.99	100	2.2	3.7	3.6	3.73	5.3
	<b>562.5</b>	41	37.4	0.99	100	2.4	3.9	3.9	3.95	5.3
	<b>587.5</b>	43	35.4	0.99	100	2.6	4.1	4.1	4.10	5.3
	<b>600.0</b>	44	34.6	0.99	100	2.7	4.2	4.2	4.20	5.3
<b>0.09</b>	<b>362.5</b>	22	62.20	0.98	100	0.8	2.3	2.3	2.40	5.6
	<b>387.5</b>	24	54.10	0.99	100	1.1	2.5	2.5	2.60	5.6
	<b>412.5</b>	26	52.60	0.99	100	1.3	2.7	2.7	2.82	5.6
	<b>437.5</b>	28	48.90	0.99	100	1.5	2.9	2.9	3.05	5.6
	<b>462.5</b>	30	45.50	0.99	100	1.7	3.2	3.2	3.25	5.6
	<b>487.5</b>	32	42.60	0.99	100	1.9	3.4	3.4	3.50	5.6
	<b>512.5</b>	34	41.75	0.99	100	2.1	3.6	3.6	3.70	5.6
	<b>537.5</b>	36	37.90	0.99	100	2.4	3.8	3.8	3.90	5.6
	<b>562.5</b>	38	35.70	0.99	100	2.6	4.1	4.1	4.15	5.6
	<b>587.5</b>	40	33.80	0.99	100	2.8	4.3	4.3	4.40	5.6
	<b>600.0</b>	41	33.10	0.99	100	2.9	4.4	4.4	4.50	5.6

<sup>1</sup>values are rounded-off to the nearest integer

<b>Table 2d</b> Lookup table for level basins, <i>CITRUS</i>										
$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.10</b>	<b>362.5</b>	21	59.6	0.99	100	0.9	2.4	2.4	2.50	5.8
	<b>387.5</b>	22	54.7	0.99	100	1.2	2.6	2.6	2.61	5.8
	<b>412.5</b>	24	50.5	0.99	100	1.4	2.9	2.8	2.92	5.8
	<b>437.5</b>	26	46.9	0.99	100	1.6	3.1	3.1	3.19	5.8
	<b>462.5</b>	28	43.7	0.99	100	1.9	3.3	3.3	3.40	5.8
	<b>487.5</b>	30	40.8	0.99	100	2.1	3.6	3.5	3.62	5.8
	<b>512.5</b>	32	38.7	0.99	100	2.3	3.8	3.7	3.82	5.8
	<b>537.5</b>	34	36.3	0.99	100	2.5	4.0	4.0	4.10	5.8
	<b>562.5</b>	36	34.3	0.99	100	2.8	4.2	4.2	4.25	5.8
	<b>587.5</b>	38	32.5	0.99	100	3.0	4.5	4.5	4.58	5.8
<b>600.0</b>	39	31.7	0.99	100	3.1	4.6	4.6	4.63	5.8	
<b>0.11</b>	<b>362.5</b>	19	57.4	0.99	100	1.0	2.5	2.5	2.60	6.1
	<b>387.5</b>	21	52.7	0.99	100	1.3	2.7	2.7	2.82	6.1
	<b>412.5</b>	23	48.6	0.99	100	1.5	3.0	3.0	3.10	6.1
	<b>437.5</b>	25	45.1	0.99	100	1.7	3.2	3.2	3.30	6.1
	<b>462.5</b>	27	42.0	0.99	100	2.0	3.4	3.4	3.52	6.1
	<b>487.5</b>	28	39.3	0.99	100	2.2	3.7	3.7	3.79	6.1
	<b>512.5</b>	30	37.2	0.99	100	2.4	3.9	3.9	4.00	6.1
	<b>537.5</b>	32	35.0	0.99	100	2.7	4.2	4.1	4.22	6.1
	<b>562.5</b>	34	33.0	0.99	100	2.9	4.4	4.4	4.50	6.1
	<b>587.5</b>	36	31.2	0.99	100	3.2	4.7	4.6	4.72	6.1
<b>600.0</b>	37	30.5	0.99	100	3.3	4.8	4.8	4.90	6.1	

<sup>1</sup>values are rounded-off to the nearest integer

<b>Table 2e</b> Lookup table for level basins, <i>CITRUS</i>										
$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{iq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.12</b>	<b>362.5</b>	18	55.4	0.99	100	1.1	2.6	2.6	2.68	6.4
	<b>387.5</b>	20	50.8	0.99	100	1.4	2.9	2.8	2.92	6.4
	<b>412.5</b>	22	46.9	0.99	100	1.6	3.1	3.1	3.18	6.4
	<b>437.5</b>	24	43.6	0.99	100	1.9	3.3	3.3	3.41	6.4
	<b>462.5</b>	25	40.6	0.99	100	2.1	3.6	3.6	3.65	6.4
	<b>487.5</b>	27	37.9	0.99	100	2.4	3.8	3.8	3.90	6.4
	<b>512.5</b>	29	35.9	0.99	100	2.6	4.1	4.0	4.10	6.4
	<b>537.5</b>	30	33.8	0.99	100	2.8	4.3	4.3	4.40	6.4
	<b>562.5</b>	32	31.9	0.99	100	3.1	4.6	4.6	4.62	6.4
	<b>587.5</b>	34	30.2	0.99	100	3.4	4.8	4.8	4.90	6.4
<b>600.0</b>	35	29.5	0.99	100	3.5	4.9	4.9	5.04	6.4	
<b>0.13</b>	<b>362.5</b>	18	53.6	0.99	100	1.2	2.7	2.7	2.77	6.6
	<b>387.5</b>	19	49.2	0.99	100	1.5	2.9	2.9	3.01	6.6
	<b>412.5</b>	21	45.4	0.99	100	1.7	3.2	3.2	3.22	6.6
	<b>437.5</b>	22	42.2	0.99	100	2.0	3.4	3.4	3.50	6.6
	<b>462.5</b>	24	39.3	0.99	100	2.2	3.7	3.7	3.78	6.6
	<b>487.5</b>	26	36.7	0.99	100	2.5	4.0	3.9	4.23	6.6
	<b>512.5</b>	27	34.8	0.99	100	2.7	4.2	4.2	4.27	6.6
	<b>537.5</b>	29	32.7	0.99	100	3.0	4.5	4.4	4.52	6.6
	<b>562.5</b>	31	30.8	0.99	100	3.3	4.7	4.7	4.80	6.6
	<b>587.5</b>	32	29.2	0.99	100	3.5	5.0	5.0	5.09	6.6
<b>600.0</b>	33	28.5	0.99	100	3.6	5.1	5.1	5.20	6.6	

<sup>1</sup>values are rounded-off to the nearest integer

<b>Table 2f</b> Lookup table for level basins, <i>CITRUS</i>										
$Q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{iq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.14</b>	<b>362.5</b>	17	52.0	0.99	100	1.3	2.8	2.8	2.85	6.8
	<b>387.5</b>	18	47.7	0.99	100	1.6	3.0	3.0	3.10	6.8
	<b>412.5</b>	20	44.0	0.99	100	1.8	3.3	3.3	3.38	6.8
	<b>437.5</b>	21	40.9	0.99	100	2.1	3.6	3.5	3.61	6.8
	<b>462.5</b>	23	38.1	0.99	100	2.3	3.8	3.8	3.90	6.8
	<b>487.5</b>	25	35.6	0.99	100	2.6	4.1	4.1	4.18	6.8
	<b>512.5</b>	26	33.7	0.99	100	2.8	4.3	4.3	4.40	6.8
	<b>537.5</b>	38	31.7	0.99	100	3.1	4.6	4.6	4.70	6.8
	<b>562.5</b>	29	29.9	0.99	100	3.4	4.9	4.9	4.96	6.8
	<b>587.5</b>	31	28.3	0.99	100	3.7	5.2	5.1	5.22	6.8
<b>600.0</b>	32	27.7	0.99	100	3.8	5.3	5.3	5.33	6.8	
<b>0.15</b>	<b>362.5</b>	16	50.6	0.99	100	1.4	2.9	2.8	2.93	7.1
	<b>387.5</b>	18	46.4	0.99	100	1.7	3.1	3.1	3.20	7.1
	<b>412.5</b>	19	42.8	0.99	100	1.9	3.4	3.4	3.44	7.1
	<b>437.5</b>	21	39.8	0.99	100	2.2	3.7	3.6	3.73	7.1
	<b>462.5</b>	23	37.0	0.99	100	2.5	3.9	3.9	4.00	7.1
	<b>487.5</b>	24	34.6	0.99	100	2.7	4.2	4.2	4.28	7.1
	<b>512.5</b>	25	32.8	0.99	100	3.0	4.4	4.4	4.50	7.1
	<b>537.5</b>	27	30.8	0.99	100	3.3	4.7	4.7	4.80	7.1
	<b>562.5</b>	28	29.1	0.99	100	3.5	5.0	5.0	5.18	7.1
	<b>587.5</b>	30	27.5	0.99	100	3.8	5.3	5.3	5.38	7.1
	<b>600.0</b>	30	26.9	0.99	100	3.9	5.4	5.4	5.50	7.1

<sup>1</sup>values are rounded-off to the nearest integer

<b>Table 2g</b> Lookup table for level basins, <i>CITRUS</i>										
$Q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{iq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.16</b>	<b>362.5</b>	16	49.2	0.99	100	1.5	2.9	2.9	3.01	7.3
	<b>387.5</b>	17	45.2	0.99	100	1.7	3.2	3.2	3.30	7.3
	<b>412.5</b>	18	41.7	0.99	100	2.0	3.5	3.5	3.55	7.3
	<b>437.5</b>	20	38.7	0.99	100	2.3	3.8	3.7	3.82	7.3
	<b>462.5</b>	21	36.1	0.99	100	2.6	4.0	4.0	4.10	7.3
	<b>487.5</b>	23	33.7	0.99	100	2.8	4.3	4.3	4.40	7.3
	<b>512.5</b>	24	31.9	0.99	100	3.1	4.6	4.5	4.62	7.3
	<b>537.5</b>	26	30.0	0.99	100	3.4	4.9	4.8	4.94	7.3
	<b>562.5</b>	27	28.3	0.99	100	3.7	5.2	5.1	5.21	7.3
	<b>587.5</b>	28	26.8	0.99	100	4.0	5.4	5.4	5.50	7.3
	<b>600.0</b>	29	26.2	0.99	100	4.1	5.6	5.6	5.62	7.3
<b>0.17</b>	<b>337.5</b>	14	51.9	0.99	100	1.3	2.8	2.8	2.85	7.5
	<b>362.5</b>	15	48.0	0.99	100	1.5	3.0	3.0	3.10	7.5
	<b>387.5</b>	16	44.1	0.99	100	1.8	3.3	3.3	3.37	7.5
	<b>412.5</b>	18	40.7	0.99	100	2.1	3.6	3.6	3.62	7.5
	<b>437.5</b>	19	37.8	0.99	100	2.4	3.9	3.8	3.92	7.5
	<b>462.5</b>	21	35.2	0.99	100	2.7	4.1	4.1	4.20	7.5
	<b>487.5</b>	22	32.9	0.99	100	3.0	4.4	4.4	4.50	7.5
	<b>512.5</b>	23	31.1	0.99	100	3.2	4.7	4.7	4.75	7.5
	<b>537.5</b>	25	29.3	0.99	100	3.5	5.0	5.0	5.02	7.5
	<b>562.5</b>	26	27.6	0.99	100	3.8	5.3	5.3	5.37	7.5
	<b>587.5</b>	27	26.2	0.99	100	4.1	5.6	5.6	5.62	7.5
	<b>600.0</b>	28	25.5	0.99	100	4.2	5.7	5.7	5.80	7.5

<sup>1</sup>values are rounded-off to the nearest integer

<b>Table 2h</b> Lookup table for level basins, <i>CITRUS</i>										
$Q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
	<b>362.5</b>	15	46.9	0.99	100	1.6	3.1	3.1	3.16	7.7
	<b>387.5</b>	16	43.0	0.99	100	1.9	3.4	3.4	3.42	7.7
	<b>412.5</b>	17	39.7	0.99	100	2.2	3.7	3.6	3.72	7.7
	<b>437.5</b>	18	37.3	0.99	100	2.4	3.9	3.9	3.98	7.7
	<b>462.5</b>	20	34.3	0.99	100	2.8	4.2	4.2	4.30	7.7
	<b>487.5</b>	21	32.1	0.99	100	3.1	4.5	4.5	4.60	7.7
	<b>512.5</b>	22	30.4	0.99	100	3.3	4.8	4.8	4.82	7.7
	<b>537.5</b>	24	28.6	0.99	100	3.6	5.1	5.1	5.18	7.7
	<b>562.5</b>	25	27.0	0.99	100	3.9	5.4	5.4	5.50	7.7
	<b>587.5</b>	27	25.5	0.99	100	4.2	5.7	5.7	5.80	7.7
	<b>600.0</b>	27	24.9	0.99	100	4.4	5.9	5.8	5.94	7.7
	<b>362.5</b>	14	45.8	0.99	100	1.7	3.2	3.2	3.22	7.9
	<b>387.5</b>	15	42.1	0.99	100	2.0	3.5	3.4	3.52	7.9
	<b>412.5</b>	17	38.8	0.99	100	2.3	3.7	3.7	3.80	7.9
	<b>437.5</b>	18	36.0	0.99	100	2.6	4.0	4.0	4.10	7.9
	<b>462.5</b>	19	33.6	0.99	100	2.9	4.3	4.3	4.40	7.9
	<b>487.5</b>	21	31.4	0.99	100	3.2	4.6	4.6	4.70	7.9
	<b>512.5</b>	22	29.7	0.99	100	3.4	4.9	4.9	5.00	7.9
	<b>537.5</b>	23	28.0	0.99	100	3.7	5.2	5.2	5.25	7.9
	<b>562.5</b>	25	26.4	0.99	100	4.1	5.5	5.5	5.50	7.9
	<b>587.5</b>	26	25.0	0.99	100	4.4	5.9	5.8	5.95	7.9
	<b>600.0</b>	26	24.4	0.99	100	4.5	6.0	6.0	6.20	7.9

<sup>1</sup>values are rounded-off to the nearest integer

<b>Table 2i</b> Lookup table for level basins, <i>CITRUS</i>										
$Q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{iq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.20</b>	<b>362.5</b>	14	44.9	0.99	100	1.8	3.2	3.2	3.30	8.1
	<b>387.5</b>	15	41.2	0.99	100	2.1	3.5	3.5	3.60	8.1
	<b>412.5</b>	16	38.0	0.99	100	2.4	3.8	3.8	3.90	8.1
	<b>437.5</b>	17	35.3	0.99	100	2.7	4.1	4.1	4.20	8.1
	<b>462.5</b>	19	32.9	0.99	100	3.0	4.4	4.4	4.50	8.1
	<b>487.5</b>	20	30.7	0.99	100	3.3	4.7	4.7	4.80	8.1
	<b>512.5</b>	21	29.1	0.99	100	3.5	5.0	5.0	5.08	8.1
	<b>537.5</b>	22	27.4	0.99	100	3.9	5.3	5.3	5.40	8.1
	<b>562.5</b>	24	25.8	0.99	100	4.2	5.7	5.6	5.80	8.1
	<b>587.5</b>	25	24.4	0.99	100	4.5	6.0	6.0	6.03	8.1
<b>600.0</b>	26	23.9	0.99	100	4.6	6.1	6.1	6.15	8.1	
<b>0.21</b>	<b>362.5</b>	13	44.0	0.99	100	1.8	3.3	3.3	3.38	8.2
	<b>387.5</b>	15	40.3	0.99	100	2.1	3.6	3.6	3.63	8.2
	<b>412.5</b>	16	37.2	0.99	100	2.4	3.9	3.9	3.97	8.2
	<b>437.5</b>	17	34.6	0.99	100	2.7	4.2	4.2	4.23	8.2
	<b>462.5</b>	18	32.2	0.99	100	3.1	4.5	4.5	4.60	8.2
	<b>487.5</b>	19	30.1	0.99	100	3.4	4.8	4.8	4.90	8.2
	<b>512.5</b>	21	28.5	0.99	100	3.6	5.1	5.1	5.20	8.2
	<b>537.5</b>	22	26.8	0.99	100	4.0	5.4	5.4	5.50	8.2
	<b>562.5</b>	23	25.3	0.99	100	4.3	5.8	5.8	5.85	8.2
	<b>587.5</b>	24	23.9	0.99	100	4.6	6.1	6.1	6.15	8.2
<b>600.0</b>	25	23.4	0.99	100	4.8	6.2	6.2	6.22	8.2	

<sup>1</sup>values are rounded-off to the nearest integer

<b>Table 2j</b> Lookup table for level basins, <i>CITRUS</i>										
$Q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.22</b>	<b>362.5</b>	13	43.1	0.99	100	1.9	3.4	3.3	3.42	8.4
	<b>387.5</b>	14	39.6	0.99	100	2.2	3.7	3.7	3.72	8.4
	<b>412.5</b>	15	36.5	0.99	100	2.5	4.0	4.0	4.02	8.4
	<b>437.5</b>	16	33.9	0.99	100	2.8	4.3	4.3	4.38	8.4
	<b>462.5</b>	18	31.6	0.99	100	3.1	4.6	4.6	4.70	8.4
	<b>487.5</b>	19	29.5	0.99	100	3.5	4.9	4.9	5.00	8.4
	<b>512.5</b>	20	27.9	0.99	100	3.7	5.2	5.2	5.30	8.4
	<b>537.5</b>	21	26.3	0.99	100	4.1	5.6	5.5	5.61	8.4
	<b>562.5</b>	23	24.8	0.99	100	4.4	5.9	5.9	5.97	8.4
	<b>587.5</b>	24	23.5	0.99	100	4.7	6.2	6.2	6.30	8.4
<b>600.0</b>	25	22.9	0.99	100	4.9	6.4	6.4	6.18	8.4	
<b>0.23</b>	<b>362.5</b>	13	42.3	0.99	100	2.0	3.4	3.4	3.50	8.6
	<b>387.5</b>	14	38.8	0.99	100	2.3	3.7	3.7	3.80	8.6
	<b>412.5</b>	15	35.8	0.99	100	2.6	4.1	4.0	4.15	8.6
	<b>437.5</b>	16	33.3	0.99	100	2.9	4.4	4.4	4.44	8.6
	<b>462.5</b>	17	31.0	0.99	100	3.2	4.7	4.7	4.78	8.6
	<b>487.5</b>	18	29.0	0.99	100	3.6	5.0	5.0	5.10	8.6
	<b>512.5</b>	19	27.4	0.99	100	3.8	5.3	5.3	5.40	8.6
	<b>537.5</b>	20	25.8	0.99	100	4.2	5.7	5.6	5.80	8.6
	<b>562.5</b>	22	24.3	0.99	100	4.5	6.0	6.0	6.03	8.6
	<b>587.5</b>	23	23.0	0.99	100	4.9	6.3	6.3	6.30	8.6
<b>600.0</b>	24	22.5	0.99	100	5.0	6.5	6.5	6.52	8.6	

<sup>1</sup>values are rounded-off to the nearest integer

<b>Table 2k</b> Lookup table for level basins, <i>CITRUS</i>										
$Q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{iq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.24</b>	<b>362.5</b>	12	41.5	0.99	100	2.0	3.5	3.5	3.48	8.8
	<b>387.5</b>	13	38.1	0.99	100	2.3	3.8	3.8	3.90	8.8
	<b>412.5</b>	15	35.2	0.99	100	2.7	4.1	4.1	4.20	8.8
	<b>437.5</b>	16	32.7	0.99	100	3.0	4.5	4.4	4.55	8.8
	<b>462.5</b>	17	30.4	0.99	100	3.3	4.8	4.8	4.84	8.8
	<b>487.5</b>	18	28.5	0.99	100	3.7	5.1	5.1	5.20	8.8
	<b>512.5</b>	19	26.9	0.99	100	3.9	5.4	5.4	5.50	8.8
	<b>537.5</b>	20	25.3	0.99	100	4.3	5.8	5.7	5.90	8.8
	<b>562.5</b>	21	23.9	0.99	100	4.6	6.1	6.1	6.15	8.8
	<b>587.5</b>	23	22.6	0.99	100	5.0	6.5	6.4	6.50	8.8
<b>600.0</b>	24	22.1	0.99	100	5.1	6.6	6.6	6.70	8.8	
<b>0.25</b>	<b>362.5</b>	12	40.8	0.99	100	2.1	3.6	3.5	3.61	8.9
	<b>387.5</b>	13	37.5	0.99	100	2.4	3.9	3.9	3.95	8.9
	<b>412.5</b>	14	34.6	0.99	100	2.7	4.2	4.2	4.30	8.9
	<b>437.5</b>	15	32.1	0.99	100	3.1	4.5	4.5	4.60	8.9
	<b>462.5</b>	16	29.9	0.99	100	3.4	4.9	4.9	4.95	8.9
	<b>487.5</b>	18	28.0	0.99	100	3.7	5.2	5.2	5.25	8.9
	<b>512.5</b>	19	26.5	0.99	100	4.0	5.5	5.5	5.60	8.9
	<b>537.5</b>	20	24.9	0.99	100	4.4	5.9	5.9	5.97	8.9
	<b>562.5</b>	21	23.5	0.99	100	4.7	6.2	6.2	6.25	8.9
	<b>587.5</b>	22	22.2	0.99	100	5.1	6.6	6.6	6.60	8.9
<b>600.0</b>	23	21.7	0.99	100	5.3	6.7	6.7	6.75	8.9	

<sup>1</sup>values are rounded-off to the nearest integer

$Q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.04</b>	<b>337.5</b>	49	63.0	0.97	100	0.8	2.3	2.2	2.3	5.1
	<b>362.5</b>	53	58.2	0.97	100	1.0	2.5	2.4	2.5	5.2
	<b>387.5</b>	58	53.4	0.97	100	1.2	2.7	2.6	2.7	5.3
	<b>412.5</b>	62	49.2	0.98	100	1.5	2.9	2.9	2.9	5.4
	<b>437.5</b>	67	45.7	0.98	100	1.7	3.2	3.1	3.2	5.4
	<b>462.5</b>	72	42.6	0.98	100	1.9	3.4	3.3	3.4	5.5
	<b>487.5</b>	77	39.8	0.98	100	2.2	3.7	3.6	3.7	5.6
	<b>512.5</b>	82	37.6	0.98	100	2.4	3.9	3.8	3.9	5.6
	<b>537.5</b>	87	35.4	0.98	100	2.6	4.1	4.0	4.1	5.7
	<b>562.5</b>	92	33.3	0.98	100	2.9	4.4	4.3	4.4	5.7
	<b>587.5</b>	97	31.6	0.98	100	3.1	4.6	4.5	4.6	5.8
	<b>600.0</b>	100	30.8	0.98	100	3.3	4.7	4.7	4.7	5.8
<b>0.05</b>	<b>337.5</b>	43	57.8	0.97	100	1.0	2.5	2.4	2.5	5.7
	<b>362.5</b>	46	53.4	0.98	100	1.2	2.7	2.6	2.7	5.8
	<b>387.5</b>	50	49.0	0.98	100	1.5	3.0	2.9	3.0	5.9
	<b>412.5</b>	54	45.2	0.98	100	1.7	3.2	3.1	3.2	5.9
	<b>437.5</b>	59	41.9	0.98	100	2.0	3.5	3.4	3.5	6.0
	<b>462.5</b>	63	39.0	0.98	100	2.3	3.7	3.7	3.7	6.1
	<b>487.5</b>	67	36.5	0.98	100	2.5	3.9	3.9	3.9	6.2
	<b>512.5</b>	71	34.5	0.98	100	2.7	4.2	4.2	4.2	6.2
	<b>537.5</b>	76	32.5	0.98	100	3.0	4.5	4.4	4.5	6.3
	<b>562.5</b>	80	30.6	0.99	100	3.3	4.8	4.7	4.8	6.4
	<b>587.5</b>	85	29.0	0.99	100	3.6	5.0	5.0	5.0	6.4
	<b>600.0</b>	87	28.3	0.99	100	3.7	5.2	5.1	5.2	6.5

<sup>1</sup>values are rounded-off to the nearest integer

$Q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.06</b>	<b>337.5</b>	38	53.8	0.98	100	1.2	2.7	2.6	2.7	6.2
	<b>362.5</b>	41	49.7	0.98	100	1.4	2.9	2.8	2.9	6.3
	<b>387.5</b>	45	45.6	0.98	100	1.7	3.2	3.1	3.2	6.4
	<b>412.5</b>	49	42.0	0.98	100	2.0	3.5	3.4	3.5	6.5
	<b>437.5</b>	52	39.0	0.98	100	2.3	3.7	3.7	3.7	6.6
	<b>462.5</b>	56	36.3	0.99	100	2.5	4.0	3.9	4.0	6.6
	<b>487.5</b>	60	34.0	0.99	100	2.8	4.3	4.2	4.3	6.7
	<b>512.5</b>	64	32.1	0.99	100	3.1	4.5	4.5	4.5	6.8
	<b>537.5</b>	68	30.2	0.99	100	3.4	4.8	4.8	4.8	6.9
	<b>562.5</b>	72	28.5	0.99	100	3.6	5.1	5.1	5.1	6.9
	<b>587.5</b>	76	27.0	0.99	100	3.9	5.4	5.4	5.4	7.0
	<b>600</b>	78	26.3	0.99	100	4.1	5.5	5.5	5.5	7.0
<b>0.07</b>	<b>337.5</b>	35	50.5	0.98	100	1.4	2.4	2.8	2.9	6.6
	<b>362.5</b>	38	46.7	0.98	100	1.6	3.1	3.0	3.1	6.7
	<b>387.5</b>	41	42.8	0.98	100	1.9	3.4	3.3	3.4	6.8
	<b>412.5</b>	44	39.5	0.98	100	2.2	3.7	3.6	3.7	6.9
	<b>437.5</b>	48	36.7	0.99	100	2.5	4.0	3.9	4.0	7.0
	<b>462.5</b>	52	34.1	0.99	100	2.8	4.3	4.2	4.3	7.1
	<b>487.5</b>	55	31.9	0.99	100	3.1	4.6	4.5	4.6	7.2
	<b>512.5</b>	58	30.2	0.99	100	3.4	4.8	4.8	4.8	7.3
	<b>537.5</b>	62	28.4	0.99	100	3.7	5.1	5.1	5.1	7.4
	<b>562.5</b>	65	26.8	0.99	100	4.0	5.4	5.4	5.4	7.5
	<b>587.5</b>	70	25.4	0.99	100	4.5	5.8	5.7	5.8	7.5
	<b>600</b>	71	24.8	0.99	100	4.4	5.9	5.8	5.9	7.6

<sup>1</sup>values are rounded-off to the nearest integer

<b>Table 3c</b> Lookup table for level basin, <i>ALFALFA</i>										
$Q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{1q}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.08</b>	<b>337.5</b>	32	47.9	0.98	100	1.6	3.0	3.0	3.0	7.1
	<b>362.5</b>	35	44.2	0.98	100	1.8	3.3	3.2	3.3	7.2
	<b>387.5</b>	38	40.6	0.99	100	2.1	3.6	3.5	3.6	7.3
	<b>412.5</b>	41	37.4	0.99	100	2.4	3.9	3.8	3.9	7.4
	<b>437.5</b>	44	34.7	0.99	100	2.7	4.2	4.1	4.2	7.5
	<b>462.5</b>	47	32.3	0.99	100	3.0	4.5	4.5	4.5	7.6
	<b>487.5</b>	51	30.2	0.99	100	3.3	4.8	4.8	4.8	7.7
	<b>512.5</b>	54	28.6	0.99	100	3.6	5.1	5.1	5.1	7.8
	<b>537.5</b>	57	26.9	0.99	100	3.9	5.4	5.4	5.4	7.9
	<b>562.5</b>	60	25.4	0.99	100	4.3	5.8	5.7	5.8	7.9
	<b>587.5</b>	64	24.0	0.99	100	4.6	6.1	6.0	6.1	8.0
<b>600.0</b>	65	23.5	0.99	100	4.8	6.2	6.2	6.2	8.1	
<b>0.09</b>	<b>337.5</b>	30	45.6	0.98	100	1.7	3.2	3.1	3.2	7.5
	<b>362.5</b>	32	42.1	0.98	100	2.0	3.4	3.4	3.4	7.6
	<b>387.5</b>	35	38.6	0.99	100	2.3	3.8	3.7	3.8	7.7
	<b>412.5</b>	38	35.7	0.99	100	2.6	4.1	4.0	4.1	7.8
	<b>437.5</b>	41	33.1	0.99	100	2.9	4.4	4.4	4.4	7.9
	<b>462.5</b>	44	30.8	0.99	100	3.3	4.7	4.7	4.7	8.0
	<b>487.5</b>	47	28.8	0.99	100	3.6	5.1	5.0	5.1	8.1
	<b>512.5</b>	50	27.3	0.99	100	3.9	5.4	5.3	5.4	8.2
	<b>537.5</b>	53	25.6	0.99	100	4.2	5.7	5.7	5.7	8.3
	<b>562.5</b>	56	24.2	0.99	100	4.6	6.0	6.0	6.0	8.4
	<b>587.5</b>	60	22.9	0.99	100	4.9	6.4	6.3	6.4	8.5
<b>600</b>	61	22.4	0.99	100	5.1	6.5	6.5	6.5	8.5	

<sup>1</sup>values are rounded-off to the nearest integer

$Q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.10</b>	<b>337.5</b>	28	43.6	0.98	100	1.9	3.3	3.3	3.3	7.8
	<b>362.5</b>	31	40.3	0.99	100	2.1	3.6	3.6	3.6	7.9
	<b>387.5</b>	33	37.0	0.99	100	2.5	3.9	3.9	3.9	8.1
	<b>412.5</b>	36	34.1	0.99	100	2.8	4.3	4.2	4.3	8.2
	<b>437.5</b>	39	31.7	0.99	100	3.1	4.6	4.6	4.6	8.3
	<b>462.5</b>	42	29.5	0.99	100	3.5	4.9	4.9	4.9	8.4
	<b>487.5</b>	45	27.6	0.99	100	3.8	5.3	5.2	5.3	8.5
	<b>512.5</b>	47	26.1	0.99	100	4.1	5.6	5.6	5.6	8.6
	<b>537.5</b>	50	24.6	0.99	100	4.5	5.9	5.9	5.9	8.7
	<b>562.5</b>	53	23.2	0.99	100	4.8	6.3	6.3	6.3	8.8
	<b>587.5</b>	56	21.9	0.99	100	5.2	6.7	6.6	6.7	8.9
	<b>600.0</b>	57	21.4	0.99	100	5.4	6.8	6.8	6.8	8.9
<b>0.11</b>	<b>337.5</b>	27	41.9	0.99	100	2.0	3.5	3.4	3.5	8.2
	<b>362.5</b>	29	38.8	0.99	100	2.3	3.8	3.7	3.7	8.3
	<b>387.5</b>	31	35.6	0.99	100	2.6	4.1	4.1	4.1	8.4
	<b>412.5</b>	34	32.8	0.99	100	3.0	4.4	4.4	4.4	8.6
	<b>437.5</b>	32	30.8	0.99	100	3.3	4.7	4.7	4.7	8.7
	<b>462.5</b>	39	28.4	0.99	100	3.7	5.1	5.1	5.1	8.8
	<b>487.5</b>	42	26.5	0.99	100	4.0	5.5	5.5	5.5	8.9
	<b>512.5</b>	45	25.1	0.99	100	4.3	5.8	5.8	5.8	9.0
	<b>537.5</b>	47	23.6	0.99	100	4.7	6.2	6.2	6.2	9.1
	<b>562.5</b>	50	22.3	0.99	100	5.1	6.6	6.5	6.6	9.2
	<b>587.5</b>	53	21.1	0.99	100	5.5	6.9	6.9	6.9	9.3
	<b>600</b>	54	20.6	0.99	100	5.6	7.1	7.1	7.1	9.3

<sup>1</sup>values are rounded-off to the nearest integer

Table 3e Lookup table for level basin, ALFALFA										
$Q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{1q}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.12</b>	<b>337.5</b>	25	40.4	0.99	100	2.1	3.6	3.5	3.6	8.5
	<b>362.5</b>	27	37.4	0.99	100	2.4	3.9	3.8	3.9	8.6
	<b>387.5</b>	30	34.3	0.99	100	2.8	4.2	4.2	4.2	8.8
	<b>412.5</b>	32	31.6	0.99	100	3.1	4.6	4.6	4.6	8.9
	<b>437.5</b>	35	29.4	0.99	100	3.5	4.9	4.9	4.9	9.0
	<b>462.5</b>	37	27.3	0.99	100	3.9	5.3	5.3	5.3	9.2
	<b>487.5</b>	40	25.6	0.99	100	4.2	5.7	5.7	5.7	9.3
	<b>512.5</b>	42	24.2	0.99	100	4.6	6.0	6.0	6.0	9.4
	<b>537.5</b>	45	22.8	0.99	100	4.9	6.4	6.4	6.4	9.5
	<b>562.5</b>	48	21.5	0.99	100	5.3	6.8	6.8	6.8	9.6
	<b>587.5</b>	50	20.3	0.99	100	5.7	7.2	7.2	7.2	9.7
	<b>600.0</b>	52	19.8	0.99	100	5.9	7.4	7.3	7.4	9.7
<b>0.13</b>	<b>337.5</b>	24	39.1	0.99	100	2.2	3.7	3.7	3.7	8.8
	<b>362.5</b>	26	36.1	0.99	100	2.6	4.0	4.0	4.0	9.0
	<b>387.5</b>	29	33.2	0.99	100	2.9	4.4	4.4	4.4	9.1
	<b>412.5</b>	31	30.6	0.99	100	3.3	4.8	4.7	4.7	9.3
	<b>437.5</b>	33	28.4	0.99	100	3.7	5.1	5.1	5.1	9.4
	<b>462.5</b>	36	26.4	0.99	100	4.0	5.5	5.5	5.5	9.5
	<b>487.5</b>	38	24.7	0.99	100	4.4	5.9	5.9	5.9	9.6
	<b>512.5</b>	40	23.4	0.99	100	4.8	6.2	6.2	6.2	9.7
	<b>537.5</b>	43	22.0	0.99	100	5.2	6.0	6.0	6.0	9.8
	<b>562.5</b>	46	20.8	0.99	100	5.6	7.0	7.0	7.0	9.9
	<b>587.5</b>	48	19.6	0.99	100	6.0	7.4	7.4	7.4	10.0
	<b>600</b>	49	19.2	0.99	100	6.1	7.6	7.6	7.6	10.1

<sup>1</sup>values are rounded-off to the nearest integer

$Q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{1q}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.14</b>	<b>337.5</b>	23	37.9	0.99	100	2.4	3.8	3.8	3.8	9.1
	<b>362.5</b>	25	35.0	0.99	100	2.7	4.2	4.1	4.2	9.3
	<b>387.5</b>	27	32.1	0.99	100	3.1	4.5	4.5	4.5	9.4
	<b>412.5</b>	30	29.6	0.99	100	3.4	4.9	4.9	4.9	9.6
	<b>437.5</b>	32	27.5	0.99	100	3.8	5.3	5.3	5.3	9.7
	<b>462.5</b>	34	25.6	0.99	100	4.2	5.7	5.7	5.7	9.8
	<b>487.5</b>	37	24.0	0.99	100	4.6	6.1	6.1	6.1	10.0
	<b>512.5</b>	38	22.7	0.99	100	5.0	6.4	6.4	6.4	10.1
	<b>537.5</b>	41	21.3	0.99	100	5.4	6.9	6.8	6.9	10.2
	<b>562.5</b>	44	20.1	0.99	100	5.8	7.3	7.2	7.3	10.3
	<b>587.5</b>	46	19.0	0.99	100	6.2	7.7	7.7	7.7	10.4
<b>600</b>	47	18.6	0.99	100	6.4	7.9	7.8	7.9	10.4	
<b>0.15</b>	<b>337.5</b>	22	36.8	0.99	100	2.5	4.0	3.9	4.0	9.4
	<b>362.5</b>	24	34.0	0.99	100	2.8	4.3	4.2	4.3	9.6
	<b>387.5</b>	26	31.2	0.99	100	3.2	4.7	4.6	4.7	9.7
	<b>412.5</b>	28	28.8	0.99	100	3.6	5.0	5.0	5.1	9.9
	<b>437.5</b>	31	26.7	0.99	100	4.0	5.5	5.4	5.5	10.0
	<b>462.5</b>	33	24.9	0.99	100	4.4	5.9	5.8	5.9	10.2
	<b>487.5</b>	35	23.3	0.99	100	4.8	6.3	6.2	6.3	10.3
	<b>512.5</b>	38	22.0	0.99	100	5.2	6.6	6.6	6.6	10.4
	<b>537.5</b>	40	20.7	0.99	100	5.6	7.1	7.0	7.1	10.5
	<b>562.5</b>	42	19.5	0.99	100	6.0	7.5	7.5	7.5	10.6
	<b>587.5</b>	44	18.5	0.99	100	6.4	7.9	7.9	7.9	10.7
<b>600</b>	45	18.1	0.99	100	6.6	8.1	8.1	8.1	10.8	

<sup>1</sup>values are rounded-off to the nearest integer

<b>Table 3g</b> Lookup table for level basin, <i>ALFALFA</i>										
$Q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{1q}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>In</i>
<b>0.16</b>	<b>337.5</b>	21	35.8	0.99	100	2.6	4.1	4.0	4.1	9.7
	<b>362.5</b>	23	33.1	0.99	100	2.9	4.4	4.4	4.4	9.9
	<b>387.5</b>	25	30.4	0.99	100	3.3	4.8	4.8	4.8	10.0
	<b>412.5</b>	27	28.0	0.99	100	3.7	5.2	5.2	5.2	10.2
	<b>437.5</b>	30	26.0	0.99	100	4.1	5.6	5.6	5.6	10.3
	<b>462.5</b>	32	24.2	0.99	100	4.6	6.0	6.0	6.0	10.5
	<b>487.5</b>	34	22.6	0.99	100	5.0	6.5	6.4	6.5	10.6
	<b>512.5</b>	36	21.4	0.99	100	5.3	6.8	6.8	6.8	10.7
	<b>537.5</b>	38	20.2	0.99	100	5.8	7.3	7.2	7.3	10.8
	<b>562.5</b>	40	19.0	0.99	100	6.2	7.7	7.7	7.7	10.9
	<b>587.5</b>	43	18.0	0.99	100	6.7	8.1	8.1	8.1	11.1
	<b>600.0</b>	44	17.6	0.99	100	6.8	8.3	8.3	8.3	11.1
<b>0.17</b>	<b>337.5</b>	21	34.9	0.99	100	2.7	4.2	4.1	4.2	10.0
	<b>362.5</b>	22	32.2	0.99	100	3.0	4.5	4.5	4.5	10.2
	<b>387.5</b>	24	29.6	0.99	100	3.5	4.9	4.9	4.9	10.3
	<b>412.5</b>	27	27.3	0.99	100	3.9	5.3	5.3	5.3	10.5
	<b>437.5</b>	29	25.3	0.99	100	4.3	5.8	5.7	5.8	10.6
	<b>462.5</b>	31	23.6	0.99	100	4.7	6.2	6.2	6.2	10.8
	<b>487.5</b>	33	22.1	0.99	100	5.2	6.6	6.6	6.6	10.9
	<b>512.5</b>	35	20.9	0.99	100	5.5	7.0	7.0	7.0	11.0
	<b>537.5</b>	37	19.6	0.99	100	6.0	7.4	7.4	7.4	11.1
	<b>562.5</b>	39	18.5	0.99	100	6.4	7.9	7.9	7.9	11.3
	<b>587.5</b>	41	17.5	0.99	100	6.9	8.3	8.3	8.3	11.4
	<b>600.0</b>	42	17.1	0.99	100	7.1	8.5	8.5	8.5	11.4

<sup>1</sup>values are rounded-off to the nearest integer

<b>Table 3h</b> Lookup table for level basin, <i>ALFALFA</i>										
$Q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.18</b>	<b>337.5</b>	20	34.1	0.99	100	2.8	4.3	4.2	4.3	10.3
	<b>362.5</b>	22	31.5	0.99	100	3.2	4.6	4.6	4.6	10.4
	<b>387.5</b>	24	28.9	0.99	100	3.6	5.1	5.0	5.1	10.6
	<b>412.5</b>	26	26.6	0.99	100	4.0	5.5	5.4	5.5	10.8
	<b>437.5</b>	28	24.7	0.99	100	4.4	5.9	5.9	5.9	10.9
	<b>462.5</b>	30	23.0	0.99	100	4.9	6.3	6.3	6.3	11.1
	<b>487.5</b>	32	21.5	0.99	100	5.3	6.8	6.8	6.8	11.2
	<b>512.5</b>	34	20.4	0.99	100	5.7	7.2	7.1	7.2	11.3
	<b>537.5</b>	36	19.2	0.99	100	6.2	7.6	7.6	7.6	11.4
	<b>562.5</b>	38	18.1	0.99	100	6.6	8.1	8.1	8.1	11.6
	<b>587.5</b>	40	17.1	0.99	100	7.1	8.6	8.5	8.6	11.7
<b>600.0</b>	41	16.7	0.99	100	7.3	8.8	8.7	8.8	11.7	
<b>0.19</b>	<b>337.5</b>	19	33.3	0.99	100	2.9	4.4	4.3	4.4	10.5
	<b>362.5</b>	21	30.7	0.99	100	3.3	4.7	4.7	4.7	10.7
	<b>387.5</b>	23	28.2	0.99	100	3.7	5.2	5.1	5.2	10.9
	<b>412.5</b>	25	26.0	0.99	100	4.1	5.6	5.6	5.6	11.0
	<b>437.5</b>	27	24.2	0.99	100	4.6	6.0	6.0	6.0	11.2
	<b>462.5</b>	29	22.5	0.99	100	5.0	6.5	6.5	6.5	11.3
	<b>487.5</b>	31	21.0	0.99	100	5.5	6.9	6.9	6.9	11.5
	<b>512.5</b>	32	19.9	0.99	100	5.9	7.3	7.3	7.3	11.6
	<b>537.5</b>	34	18.7	0.99	100	6.3	7.8	7.8	7.8	11.7
	<b>562.5</b>	37	17.7	0.99	100	6.8	8.3	8.3	8.3	11.9
	<b>587.5</b>	39	16.7	0.99	100	7.3	8.8	8.7	8.8	12.0
<b>600</b>	40	16.3	0.99	100	7.5	9.0	8.9	9.0	12.0	

<sup>1</sup>values are rounded-off to the nearest integer

<b>Table 3i</b> Lookup table for level basin, <i>ALFALFA</i>										
$Q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{1q}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>In</i>
<b>0.20</b>	<b>337.5</b>	19	32.5	0.99	100	3.0	4.5	4.4	4.5	10.8
	<b>362.5</b>	20	30.1	0.99	100	3.4	4.9	4.8	4.9	10.9
	<b>387.5</b>	22	27.6	0.99	100	3.8	5.3	5.3	5.3	11.1
	<b>412.5</b>	24	25.5	0.99	100	4.3	5.7	5.7	5.7	11.3
	<b>437.5</b>	26	23.6	0.99	100	4.7	6.2	6.2	6.2	11.4
	<b>462.5</b>	28	22.0	0.99	100	5.2	6.6	6.6	6.6	11.6
	<b>487.5</b>	30	20.6	0.99	100	5.6	7.1	7.1	7.1	11.7
	<b>512.5</b>	32	19.5	0.99	100	6.0	7.5	7.5	7.5	11.9
	<b>537.5</b>	33	18.3	0.99	100	6.5	8.0	8.0	8.0	12.0
	<b>562.5</b>	36	17.3	0.99	100	7.0	8.5	8.4	8.5	12.1
	<b>587.5</b>	38	16.4	0.99	100	7.5	8.9	8.9	8.9	12.3
<b>600</b>	39	16.0	0.99	100	7.7	9.2	9.1	9.2	12.3	
<b>0.21</b>	<b>337.5</b>	18	31.9	0.99	100	3.1	4.6	4.5	4.6	11.0
	<b>362.5</b>	20	29.5	0.99	100	3.5	5.0	4.9	5.0	11.2
	<b>387.5</b>	22	27.0	0.99	100	3.9	5.4	5.4	5.4	11.4
	<b>412.5</b>	23	24.9	0.99	100	4.4	5.9	5.8	5.9	11.6
	<b>437.5</b>	25	23.1	0.99	100	4.8	6.3	6.3	6.3	11.7
	<b>462.5</b>	27	38.3	0.99	100	5.3	6.8	6.8	6.8	11.9
	<b>487.5</b>	29	20.2	0.99	100	5.8	7.2	7.2	7.2	12.0
	<b>512.5</b>	31	19.1	0.99	100	6.2	7.7	7.6	7.7	12.1
	<b>537.5</b>	33	17.9	0.99	100	6.7	8.2	8.1	8.2	12.3
	<b>562.5</b>	35	16.9	0.99	100	7.2	8.7	8.6	8.7	12.4
	<b>587.5</b>	36	16.0	0.99	100	7.7	9.1	9.1	9.1	12.5
<b>600</b>	37	15.6	0.99	100	7.9	9.4	9.3	9.4	12.6	

<sup>1</sup>values are rounded-off to the nearest integer

$Q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{1q}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>In</i>
<b>0.22</b>	<b>337.5</b>	18	31.2	0.99	100	3.2	4.7	4.6	4.7	11.3
	<b>362.5</b>	19	28.9	0.99	100	3.6	5.1	5.0	5.1	11.4
	<b>387.5</b>	21	26.5	0.99	100	4.0	5.5	5.5	5.5	11.6
	<b>412.5</b>	23	24.4	0.99	100	4.5	6.0	6.0	6.0	11.8
	<b>437.5</b>	25	22.7	0.99	100	5.0	6.4	6.4	6.4	12.0
	<b>462.5</b>	26	21.1	0.99	100	5.4	6.9	6.9	6.9	12.1
	<b>487.5</b>	28	19.8	0.99	100	5.9	7.4	7.4	7.4	12.3
	<b>512.5</b>	30	18.7	0.99	100	6.3	7.8	7.8	7.8	12.4
	<b>537.5</b>	32	17.6	0.99	100	6.8	8.3	8.3	8.3	12.5
	<b>562.5</b>	34	16.6	0.99	100	7.4	8.8	8.8	8.8	12.7
	<b>587.5</b>	36	15.7	0.99	100	7.9	9.3	9.3	9.3	12.8
<b>600.0</b>	37	15.3	0.99	100	8.1	9.5	9.5	9.5	12.9	
<b>0.23</b>	<b>337.5</b>	17	30.6	0.99	100	3.3	4.8	4.7	4.8	11.5
	<b>362.5</b>	19	28.3	0.99	100	3.7	5.1	5.1	5.1	11.7
	<b>387.5</b>	21	26.0	0.99	100	4.1	5.6	5.6	5.6	11.8
	<b>412.5</b>	22	24.0	0.99	100	4.6	6.1	6.1	6.1	12.0
	<b>437.5</b>	24	22.3	0.99	100	5.1	6.6	6.5	6.6	12.2
	<b>462.5</b>	26	20.7	0.99	100	5.6	7.1	7.0	7.1	12.4
	<b>487.5</b>	28	19.4	0.99	100	6.1	7.5	7.5	7.5	12.5
	<b>512.5</b>	29	18.3	0.99	100	6.5	8.0	8.0	8.0	12.7
	<b>537.5</b>	31	17.2	0.99	100	7.0	8.5	8.5	8.5	12.8
	<b>562.5</b>	33	16.3	0.99	100	7.5	9.0	9.0	9.0	12.9
	<b>587.5</b>	35	15.4	0.99	100	8.0	9.5	9.5	9.5	13.1
<b>600.0</b>	36	15.0	0.99	100	8.3	9.7	9.7	9.7	13.1	

<sup>1</sup>values are rounded-off to the nearest integer

$Q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{1q}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>In</i>	<i>in</i>	<i>in</i>
<b>0.24</b>	<b>337.5</b>	17	30.1	0.99	100	3.4	4.8	4.8	4.8	11.7
	<b>362.5</b>	18	27.8	0.99	100	3.8	5.2	5.2	5.2	11.9
	<b>387.5</b>	20	25.5	0.99	100	4.3	5.7	5.7	5.7	12.1
	<b>412.5</b>	22	23.5	0.99	100	4.7	6.2	6.2	6.2	12.3
	<b>437.5</b>	23	21.8	0.99	100	5.2	6.7	6.7	6.7	12.5
	<b>462.5</b>	25	20.3	0.99	100	5.7	7.2	7.2	7.2	12.6
	<b>487.5</b>	27	19.0	0.99	100	6.2	7.7	7.7	7.7	12.8
	<b>512.5</b>	28	18.0	0.99	100	6.7	8.8	8.1	8.1	12.9
	<b>537.5</b>	30	16.9	0.99	100	7.2	8.6	8.6	8.6	13.1
	<b>562.5</b>	32	16.0	0.99	100	7.7	9.2	9.2	9.2	13.2
	<b>587.5</b>	34	15.1	0.99	100	8.2	9.7	9.7	9.7	13.3
	<b>600.0</b>	35	14.8	0.99	100	8.4	9.9	9.9	9.9	13.4
<b>0.25</b>	<b>337.5</b>	17	29.6	0.99	100	3.5	4.9	4.9	4.9	12.0
	<b>362.5</b>	18	27.3	0.99	100	3.9	5.3	5.3	5.3	12.1
	<b>387.5</b>	20	25.1	0.99	100	4.4	5.8	5.8	5.8	12.3
	<b>412.5</b>	21	23.1	0.99	100	4.8	6.3	6.3	6.3	12.5
	<b>437.5</b>	23	21.5	0.99	100	5.3	6.8	6.8	6.8	12.7
	<b>462.5</b>	25	20.0	0.99	100	5.8	7.3	7.3	7.3	12.9
	<b>487.5</b>	26	18.7	0.99	100	6.4	7.8	7.8	7.8	13.0
	<b>512.5</b>	28	17.7	0.99	100	6.8	8.3	8.2	8.3	13.2
	<b>537.5</b>	30	16.6	0.99	100	7.3	8.8	8.8	8.8	13.3
	<b>562.5</b>	31	15.7	0.99	100	7.9	9.3	9.3	9.3	13.5
	<b>587.5</b>	33	14.9	0.99	100	8.4	9.9	9.8	9.8	13.6
	<b>600.0</b>	34	14.5	0.99	100	8.6	10.1	10.1	10.1	13.7

<sup>1</sup>values are rounded-off to the nearest integer



<b>Table 4a</b> Lookup table for basins with a bed slope of 0.1%, <i>CITRUS</i>										
<i>Qo</i>	<i>Lco</i>	<i>tco</i> <sup>1</sup>	<i>Ea</i>	<i>Dulq</i>	<i>Er</i>	<i>Dp</i>	<i>Dav</i>	<i>Dmin</i>	<i>Dapp</i>	<i>Ymax</i>
<i>cfs/ft</i>	-	<i>min</i>	%	%	%	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.04</b>	<b>337.5</b>	28	75.0	0.51	68.9	0.3	1.3	0.6	1.3	2.9
	<b>362.5</b>	31	69.2	0.41	68.9	0.4	1.4	0.1	1.4	3.2
	<b>387.5</b>	33	66.5	0.42	71.4	0.5	1.5	0.5	1.5	3.4
	<b>412.5</b>	35	64.2	0.41	73.5	0.5	1.6	0.6	1.6	3.7
	<b>437.5</b>	38	61.0	0.39	74.6	0.6	1.7	0.5	1.8	3.9
	<b>462.5</b>	40	58.3	0.36	76.0	0.7	1.9	0.4	1.9	4.1
	<b>487.5</b>	43	56.7	0.36	78.6	0.8	2.0	0.6	2.0	4.3
	<b>512.5</b>	45	53.8	0.33	78.8	0.9	2.1	0.5	2.1	4.5
	<b>537.5</b>	48	52.2	0.32	80.7	1.0	2.2	0.6	2.2	4.7
	<b>562.5</b>	50	50.4	0.32	82.1	1.1	2.3	0.7	2.4	4.9
	<b>587.5</b>	53	48.9	0.31	83.6	1.2	2.5	0.7	2.5	5.0
<b>600.0</b>	54	48.1	0.30	84.0	1.3	2.5	0.7	2.5	5.1	
<b>0.05</b>	<b>337.5</b>	25	69.4	0.45	70.1	0.4	1.4	0.5	1.4	3.3
	<b>362.5</b>	27	64.9	0.36	71.1	0.5	1.6	0.1	1.6	3.5
	<b>387.5</b>	29	62.0	0.38	73.3	0.6	1.7	0.4	1.7	3.8
	<b>412.5</b>	31	60.3	0.38	76.1	0.7	1.8	0.6	1.8	4.0
	<b>437.5</b>	33	56.7	0.34	76.4	0.8	1.9	0.5	1.9	4.2
	<b>462.5</b>	35	54.8	0.35	78.8	0.9	2.1	0.6	2.1	4.4
	<b>487.5</b>	38	52.9	0.32	80.8	1.0	2.2	0.6	2.2	4.7
	<b>512.5</b>	40	50.1	0.29	80.9	1.1	2.3	0.5	2.3	4.9
	<b>537.5</b>	42	48.7	0.29	83.0	1.2	2.5	0.7	2.5	5.1
	<b>562.5</b>	44	46.6	0.27	83.7	1.4	2.6	0.5	2.6	5.2
	<b>587.5</b>	46	45.2	0.26	85.2	1.5	2.7	0.7	2.7	5.4
<b>600.0</b>	47	44.6	0.26	85.9	1.5	2.8	0.7	2.8	5.5	

<sup>1</sup>values are rounded-off to the nearest integer

<b>Table 4b</b> Lookup table for basins with a bed slope of 0.1%, <i>CITRUS</i>										
$Q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	-	<i>min</i>	%	%	%	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.06</b>	<b>337.5</b>	22	64.7	0.36	70.7	0.5	1.6	0.1	1.6	3.5
	<b>362.5</b>	24	61.6	0.37	73.0	0.6	1.7	0.5	1.7	3.8
	<b>387.5</b>	26	58.5	0.34	74.9	0.7	1.8	0.4	1.8	4.1
	<b>412.5</b>	28	56.3	0.34	76.9	0.8	2.0	0.5	2.0	4.3
	<b>437.5</b>	30	53.0	0.28	77.4	1.0	2.1	0.3	2.1	4.5
	<b>462.5</b>	32	51.1	0.29	79.6	1.1	2.2	0.4	2.2	4.8
	<b>487.5</b>	34	49.6	0.29	82.1	1.2	2.4	0.6	2.4	5.0
	<b>512.5</b>	36	47.5	0.28	83.2	1.3	2.5	0.6	2.5	5.2
	<b>537.5</b>	38	45.8	0.27	84.7	1.4	2.7	0.6	2.7	5.4
	<b>562.5</b>	40	43.9	0.24	85.5	1.6	2.8	0.5	2.8	5.6
	<b>587.5</b>	43	41.7	0.24	87.1	1.7	3.0	0.5	3.0	5.8
<b>0.07</b>	<b>337.5</b>	21	62.2	0.37	72.8	0.6	1.7	0.4	1.7	3.8
	<b>362.5</b>	22	58.7	0.34	74.5	0.7	1.8	0.4	1.8	4.1
	<b>387.5</b>	24	56.4	0.34	77.4	0.8	2.0	0.6	2.0	4.3
	<b>412.5</b>	26	53.4	0.31	78.1	1.0	2.1	0.5	2.1	4.5
	<b>437.5</b>	28	50.8	0.28	79.5	1.1	2.3	0.4	2.3	4.8
	<b>462.5</b>	29	48.6	0.26	81.1	1.2	2.4	0.4	2.4	5.0
	<b>487.5</b>	31	46.7	0.26	82.8	1.3	2.6	0.5	2.6	5.2
	<b>512.5</b>	33	45.1	0.25	84.6	1.5	2.7	0.6	2.7	5.4
	<b>537.5</b>	35	43.6	0.25	86.4	1.6	2.9	0.6	2.9	5.7
	<b>562.5</b>	37	41.7	0.24	87.1	1.7	3.0	0.5	3.0	5.9
	<b>587.5</b>	39	40.6	0.25	89.0	1.9	3.2	0.7	3.2	6.0
	<b>600.0</b>	40	39.9	0.26	89.4	1.9	3.2	0.7	3.3	6.1

<sup>1</sup>values are rounded-off to the nearest integer

<b>Table 4c</b> Lookup table for basins with a bed slope of 0.1%, <i>CITRUS</i>										
$Q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	-	<i>min</i>	%	%	%	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.08</b>	<b>337.5</b>	19	59.8	0.36	74.3	0.7	1.8	0.5	1.8	4.0
	<b>362.5</b>	21	56.3	0.33	75.8	0.8	1.9	0.5	1.9	4.3
	<b>387.5</b>	22	53.4	0.30	77.7	0.9	2.1	0.5	2.1	4.5
	<b>412.5</b>	24	51.0	0.28	79.2	1.1	2.2	0.4	2.2	4.8
	<b>437.5</b>	26	48.7	0.26	80.9	1.2	2.4	0.3	2.4	5.0
	<b>462.5</b>	27	46.7	0.26	82.8	1.3	2.6	0.5	2.6	5.2
	<b>487.5</b>	29	44.6	0.24	84.0	1.5	2.7	0.4	2.7	5.5
	<b>512.5</b>	31	42.9	0.23	85.5	1.6	2.9	0.4	2.9	5.7
	<b>537.5</b>	32	41.8	0.25	88.1	1.8	3.1	0.6	3.1	5.9
	<b>562.5</b>	34	40.1	0.25	89.0	1.9	3.2	0.6	3.2	6.1
	<b>587.5</b>	36	38.7	0.26	90.2	2.1	3.4	0.5	3.4	6.3
	<b>600.0</b>	37	38.3	0.27	91.2	2.1	3.5	0.6	3.5	6.4
<b>0.09</b>	<b>337.5</b>	18	56.7	0.30	74.2	0.8	1.9	0.2	1.9	4.2
	<b>362.5</b>	19	54.2	0.30	77.0	0.9	2.0	0.4	2.0	4.5
	<b>387.5</b>	21	51.2	0.28	78.6	1.0	2.2	0.4	2.2	4.7
	<b>412.5</b>	22	49.3	0.28	80.7	1.2	2.4	0.5	2.4	5.0
	<b>437.5</b>	24	46.8	0.25	82.0	1.3	2.5	0.5	2.5	5.2
	<b>462.5</b>	26	44.8	0.23	83.8	1.5	2.7	0.4	2.7	5.5
	<b>487.5</b>	27	43.2	0.24	85.9	1.6	2.9	0.6	2.9	5.7
	<b>512.5</b>	29	41.8	0.25	88.0	1.8	3.1	0.6	3.1	5.9
	<b>537.5</b>	30	39.8	0.24	88.5	1.9	3.2	0.4	3.2	6.1
	<b>562.5</b>	32	38.7	0.27	90.6	2.1	3.4	0.6	3.4	6.3
	<b>587.5</b>	34	37.5	0.28	92.3	2.2	3.6	0.6	3.6	6.5
	<b>600.0</b>	34	36.9	0.29	92.7	2.3	3.7	0.6	3.7	6.6

<sup>1</sup>values are rounded-off to the nearest integer

<b>Table 4d</b> Lookup table for basins with a bed slope of 0.1%, <i>CITRUS</i>										
$Q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{iq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	-	<i>min</i>	%	%	%	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>In</i>
<b>0.10</b>	<b>337.5</b>	17	56.1	0.33	77.0	0.9	2.0	0.6	2.0	4.3
	<b>362.5</b>	18	52.6	0.30	78.3	1.0	2.1	0.5	2.1	4.6
	<b>387.5</b>	20	49.6	0.27	79.8	1.1	2.3	0.5	2.3	4.9
	<b>412.5</b>	21	47.4	0.25	81.4	1.3	2.5	0.4	2.5	5.1
	<b>437.5</b>	23	45.3	0.23	83.3	1.4	2.7	0.4	2.7	5.4
	<b>462.5</b>	24	43.9	0.25	86.1	1.6	2.9	0.6	2.8	5.6
	<b>487.5</b>	26	41.5	0.23	86.4	1.7	3.0	0.5	3.0	5.9
	<b>512.5</b>	27	40.2	0.25	88.8	1.9	3.2	0.6	3.2	6.1
	<b>537.5</b>	29	38.8	0.26	90.5	2.1	3.4	0.6	3.4	6.3
	<b>562.5</b>	30	37.4	0.28	92.0	2.2	3.6	0.6	3.6	6.6
	<b>587.5</b>	32	36.1	0.30	93.3	2.4	3.8	0.6	3.8	6.8
<b>600.0</b>	32	35.5	0.31	93.7	2.5	3.8	0.4	3.8	6.8	
<b>0.11</b>	<b>337.5</b>	16	53.5	0.29	76.6	0.9	2.1	0.3	2.1	4.5
	<b>362.5</b>	17	51.6	0.29	79.5	1.1	2.2	0.6	2.2	4.7
	<b>387.5</b>	19	48.3	0.26	80.6	1.2	2.4	0.4	2.4	5.0
	<b>412.5</b>	20	45.8	0.24	82.4	1.4	2.6	0.4	2.6	5.3
	<b>437.5</b>	22	43.7	0.22	74.1	1.5	2.8	0.3	2.8	5.6
	<b>462.5</b>	23	42.4	0.24	87.2	1.7	3.0	0.6	3.0	5.8
	<b>487.5</b>	24	40.1	0.23	87.7	1.9	3.2	0.4	3.2	6.1
	<b>512.5</b>	26	39.0	0.25	89.7	2.0	3.3	0.5	3.3	6.3
	<b>537.5</b>	27	37.7	0.28	91.7	2.2	3.6	0.6	3.5	6.5
	<b>562.5</b>	29	36.2	0.30	92.9	2.4	3.7	0.6	3.7	6.7
	<b>587.5</b>	30	35.1	0.33	94.7	2.5	3.9	0.6	3.9	7.0
<b>600.0</b>	31	34.6	0.34	95.4	2.6	4.0	0.6	4.0	7.0	

<sup>1</sup>values are rounded-off to the nearest integer

<b>Table 4e</b> Lookup table for basins with a bed slope of 0.1%, <i>CITRUS</i>										
$Q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{la}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	-	<i>min</i>	%	%	%	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.12</b>	<b>337.5</b>	15	52.2	0.29	77.7	1.0	2.1	0.4	2.1	4.6
	<b>362.5</b>	16	49.4	0.26	79.1	1.1	2.3	0.4	2.3	4.9
	<b>387.5</b>	18	46.8	0.24	81.3	1.3	2.5	0.3	2.5	5.2
	<b>412.5</b>	19	44.8	0.24	83.8	1.5	2.7	0.5	2.7	5.5
	<b>437.5</b>	21	42.5	0.22	85.2	1.6	2.9	0.4	2.9	5.7
	<b>462.5</b>	22	40.6	0.23	86.9	1.8	3.1	0.3	3.1	6.0
	<b>487.5</b>	23	38.9	0.24	88.5	2.0	3.3	0.2	3.3	6.2
	<b>512.5</b>	25	37.7	0.26	90.3	2.1	3.5	0.4	3.5	6.4
	<b>537.5</b>	26	36.6	0.29	92.7	2.3	3.7	0.6	3.7	6.7
	<b>562.5</b>	27	35.3	0.32	94.4	2.5	3.9	0.6	3.9	6.9
	<b>587.5</b>	29	34.1	0.35	95.8	2.7	4.1	0.6	4.1	7.1
<b>600.0</b>	30	33.7	0.36	96.8	2.8	4.2	0.6	4.2	7.2	
<b>0.13</b>	<b>312.5</b>	13	53.9	0.29	75.9	0.9	2.0	0.3	2.0	4.6
	<b>337.5</b>	15	51.5	0.29	79.5	1.1	2.2	0.6	2.2	4.8
	<b>362.5</b>	16	48.5	0.26	80.6	1.2	2.4	0.4	2.4	5.0
	<b>387.5</b>	17	45.7	0.23	82.3	1.4	2.6	0.4	2.6	5.3
	<b>412.5</b>	18	43.4	0.22	84.2	1.6	2.8	0.3	2.8	5.6
	<b>437.5</b>	20	41.4	0.22	86.0	1.7	3.0	0.3	3.0	5.9
	<b>462.5</b>	21	39.7	0.24	88.2	1.9	3.2	0.4	3.2	6.1
	<b>487.5</b>	22	38.3	0.26	90.5	2.1	3.4	0.6	2.1	6.4
	<b>512.5</b>	24	37.1	0.29	92.2	2.3	3.6	0.6	3.6	6.6
	<b>537.5</b>	25	35.6	0.31	93.6	2.4	3.8	0.4	3.8	6.9
	<b>562.5</b>	26	34.4	0.34	95.4	2.6	4.0	0.6	4.0	7.1
<b>587.5</b>	28	33.3	0.37	97.1	2.8	4.3	0.7	4.3	7.3	
<b>600.0</b>	29	32.8	0.38	97.8	2.9	4.3	0.8	4.3	7.4	

<sup>1</sup>values are rounded-off to the nearest integer

<b>Table 4f</b> Lookup table for basins with a bed slope of 0.1%, <i>CITRUS</i>										
$Q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{la}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	-	<i>min</i>	%	%	%	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.14</b>	<b>337.5</b>	14	49.6	0.26	79.2	1.1	2.3	0.3	2.3	4.9
	<b>362.5</b>	15	47.0	0.23	80.8	1.3	2.5	0.3	2.5	5.2
	<b>387.5</b>	16	44.9	0.23	83.6	1.5	2.7	0.5	2.7	5.5
	<b>412.5</b>	18	42.4	0.22	85.2	1.6	2.9	0.4	2.9	5.7
	<b>437.5</b>	19	40.4	0.23	86.9	1.8	3.1	0.3	3.1	6.0
	<b>462.5</b>	20	38.9	0.25	89.3	2.0	3.3	0.5	3.3	6.3
	<b>487.5</b>	21	37.5	0.28	91.7	2.2	3.6	0.6	3.6	6.5
	<b>512.5</b>	23	36.2	0.30	93.1	2.4	3.7	0.6	3.7	6.8
	<b>537.5</b>	24	34.9	0.33	95.0	2.6	4.0	0.6	4.0	7.0
	<b>562.5</b>	25	33.6	0.36	96.5	2.8	4.2	0.6	4.2	7.2
	<b>587.5</b>	27	32.5	0.39	98.1	3.0	4.4	0.8	4.4	7.5
	<b>600.0</b>	28	31.9	0.41	98.4	3.0	4.5	0.9	4.5	7.6
<b>0.15</b>	<b>337.5</b>	14	48.5	0.25	79.8	1.2	2.4	0.4	2.4	5.0
	<b>362.5</b>	15	46.1	0.23	81.7	1.4	2.6	0.4	2.6	5.3
	<b>387.5</b>	16	43.6	0.22	83.8	1.5	2.8	0.3	2.8	5.6
	<b>412.5</b>	17	41.4	0.22	85.8	1.7	3.0	0.2	3.0	5.9
	<b>437.5</b>	18	39.7	0.24	88.2	1.9	3.2	0.4	3.2	6.2
	<b>462.5</b>	19	37.8	0.25	89.7	2.1	3.4	0.3	3.5	6.4
	<b>487.5</b>	21	36.6	0.29	92.4	2.3	3.7	0.5	3.7	6.7
	<b>512.5</b>	22	35.5	0.32	94.3	2.5	3.9	0.6	3.9	6.9
	<b>537.5</b>	23	34.1	0.35	95.9	2.7	4.1	0.6	4.1	7.2
	<b>562.5</b>	24	32.9	0.38	97.6	2.9	4.3	0.8	4.3	7.4
	<b>587.5</b>	26	31.7	0.41	98.9	3.1	4.6	1.0	4.6	7.6
	<b>600.0</b>	27	31.1	0.42	99.1	3.2	4.7	1.1	4.7	7.7

<sup>1</sup>values are rounded-off to the nearest integer

<b>Table 4g</b> Lookup table for basins with a bed slope of 0.1%, <i>CITRUS</i>										
$Q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{la}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	-	<i>min</i>	%	%	%	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.16</b>	<b>337.5</b>	13.04	48.1	0.26	81.6	1.3	2.5	0.6	2.5	5.1
	<b>362.5</b>	14.04	45.3	0.23	82.7	1.4	2.6	0.4	2.6	5.4
	<b>387.5</b>	15.22	42.8	0.22	84.7	1.6	2.9	0.4	2.9	5.7
	<b>412.5</b>	16.41	40.6	0.22	86.7	1.8	3.1	0.3	3.1	6.0
	<b>437.5</b>	17.58	38.7	0.24	88.5	2.0	3.3	0.2	3.3	6.3
	<b>462.5</b>	18.80	37.5	0.28	91.7	2.2	3.6	0.6	3.6	6.6
	<b>487.5</b>	20.00	35.8	0.30	93.1	2.4	3.8	0.3	3.8	6.8
	<b>512.5</b>	21.03	34.8	0.33	95.2	2.6	4.0	0.6	4.0	7.0
	<b>537.5</b>	22.26	33.5	0.37	97.0	2.8	4.2	0.7	4.2	7.3
	<b>562.5</b>	23.50	32.2	0.40	98.4	3.0	4.5	0.9	4.5	7.5
	<b>587.5</b>	24.71	30.9	0.43	99.3	3.2	4.7	1.1	4.7	7.8
<b>600.0</b>	25.25	30.3	0.44	99.5	3.3	4.8	1.2	4.8	7.9	
<b>0.17</b>	<b>337.5</b>	12.61	46.5	0.23	81.0	1.3	2.5	0.3	2.5	5.3
	<b>362.5</b>	13.58	44.9	0.24	84.3	1.5	2.7	0.6	2.7	5.5
	<b>387.5</b>	14.73	42.1	0.22	85.7	1.7	3.0	0.4	3.0	5.8
	<b>412.5</b>	15.88	39.9	0.23	87.6	1.9	3.2	0.4	3.2	6.1
	<b>437.5</b>	17.01	38.0	0.25	89.3	2.1	3.4	0.3	3.4	6.4
	<b>462.5</b>	18.18	36.6	0.28	92.0	2.3	3.7	0.2	3.7	6.7
	<b>487.5</b>	19.36	35.3	0.32	94.5	2.5	3.9	0.6	3.9	6.9
	<b>512.5</b>	20.36	34.1	0.35	96.0	2.7	4.1	0.6	4.1	7.2
	<b>537.5</b>	21.56	32.8	0.38	97.7	2.9	4.3	0.8	4.3	7.4
	<b>562.5</b>	22.76	31.5	0.42	99.1	3.1	4.6	1.0	4.6	7.7
	<b>587.5</b>	23.93	30.1	0.44	99.6	3.4	4.8	1.2	4.8	7.9
<b>600.0</b>	24.45	29.5	0.46	99.7	3.5	4.9	1.4	4.9	8.0	

<sup>1</sup>values are rounded-off to the nearest integer

<b>Table 4h</b> Lookup table for basins with a bed slope of 0.1%, <i>CITRUS</i>										
$Q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{la}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	-	<i>min</i>	%	%	%	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.18</b>	<b>337.5</b>	12	45.8	0.23	82.0	1.4	2.6	0.4	2.6	5.5
	<b>362.5</b>	13	43.5	0.22	83.8	1.6	2.8	0.3	2.8	5.6
	<b>387.5</b>	14	41.1	0.21	85.9	1.8	3.0	0.3	3.0	5.9
	<b>412.5</b>	15	39.7	0.25	89.5	2.0	3.3	0.6	3.3	6.2
	<b>437.5</b>	17	37.5	0.26	90.5	2.2	3.5	0.4	3.5	6.5
	<b>462.5</b>	18	36.0	0.30	92.9	2.4	3.8	0.3	3.8	6.8
	<b>487.5</b>	19	34.7	0.33	95.4	2.6	4.0	0.6	4.0	7.1
	<b>512.5</b>	20	33.5	0.37	96.9	2.8	4.2	0.7	4.2	7.3
	<b>537.5</b>	21	32.1	0.40	98.2	3.0	4.5	0.9	4.5	7.6
	<b>562.5</b>	22	30.8	0.43	99.5	3.3	4.7	1.1	4.7	7.8
	<b>587.5</b>	23	29.4	0.46	99.9	3.5	5.0	1.4	5.0	8.1
	<b>600.0</b>	24	28.8	0.47	100.0	3.6	5.1	1.5	5.1	8.2
<b>0.19</b>	<b>337.5</b>	12	45.2	0.23	82.9	1.4	2.7	0.4	2.7	5.7
	<b>362.5</b>	13	42.8	0.22	84.6	1.6	2.9	0.4	2.9	5.7
	<b>387.5</b>	14	40.4	0.22	86.6	1.8	3.1	0.3	3.1	6.0
	<b>412.5</b>	15	38.4	0.24	88.7	2.0	3.4	0.3	3.4	6.3
	<b>437.5</b>	16	37.0	0.28	91.6	2.2	3.6	0.5	3.6	6.6
	<b>462.5</b>	17	35.5	0.31	93.9	2.5	3.9	0.6	3.9	6.9
	<b>487.5</b>	18	34.1	0.35	96.1	2.7	4.1	0.6	4.1	7.2
	<b>512.5</b>	19	32.9	0.38	97.6	2.9	4.3	0.8	4.3	7.4
	<b>537.5</b>	20	31.5	0.41	98.8	3.1	4.6	1.0	4.6	7.7
	<b>562.5</b>	21	30.0	0.45	99.4	3.4	4.8	1.3	4.8	7.9
	<b>587.5</b>	23	28.6	0.47	99.7	3.6	5.1	1.5	5.1	8.2
	<b>600.0</b>	24	28.0	0.48	99.7	3.7	5.2	1.6	5.2	8.3

<sup>1</sup>values are rounded-off to the nearest integer

<b>Table 4i</b> Lookup table for basins with a bed slope of 0.1%, <i>CITRUS</i>										
$Q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{la}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	-	<i>Min</i>	%	%	%	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.21</b>	<b>337.5</b>	12	44.8	0.24	84.1	1.5	2.7	0.6	2.7	5.8
	<b>362.5</b>	13	42.2	0.22	85.4	1.7	2.9	0.4	2.9	5.9
	<b>387.5</b>	14	40.0	0.23	87.7	1.9	3.2	0.4	3.2	6.1
	<b>412.5</b>	15	37.9	0.25	89.7	2.1	3.4	0.3	3.4	6.4
	<b>437.5</b>	16	36.3	0.29	92.1	2.3	3.7	0.3	3.7	6.7
	<b>462.5</b>	17	35.0	0.33	94.8	2.5	3.9	0.5	3.9	7.0
	<b>487.5</b>	18	33.5	0.36	96.7	2.8	4.2	0.6	4.2	7.3
	<b>512.5</b>	19	32.3	0.40	98.1	3.0	4.4	0.9	4.4	7.5
	<b>537.5</b>	20	30.9	0.43	99.4	3.2	4.7	1.1	4.7	7.8
	<b>562.5</b>	21	29.4	0.46	99.8	3.5	5.0	1.4	5.0	8.1
	<b>587.5</b>	22	28.0	0.48	100.0	3.7	5.2	1.6	5.2	8.3
	<b>600.0</b>	23	27.4	0.50	100.0	3.9	5.3	1.7	5.3	8.5
<b>0.22</b>	<b>337.5</b>	11	43.6	0.21	83.7	1.5	2.8	0.3	2.8	6.0
	<b>362.5</b>	12	41.3	0.21	85.4	1.7	3.0	0.2	3.0	6.0
	<b>387.5</b>	13	39.7	0.25	89.1	2.0	3.3	0.5	3.3	6.2
	<b>412.5</b>	14	37.4	0.26	90.5	2.2	3.5	0.4	3.5	6.5
	<b>437.5</b>	15	35.8	0.30	92.8	2.4	3.8	0.3	3.8	6.8
	<b>462.5</b>	16	34.4	0.34	95.4	2.6	4.0	0.5	4.0	7.1
	<b>487.5</b>	17	33.0	0.38	97.5	2.9	4.3	0.7	4.3	7.4
	<b>512.5</b>	18	31.8	0.41	98.8	3.1	4.5	1.0	4.5	7.6
	<b>537.5</b>	19	30.2	0.44	99.3	3.3	4.8	1.2	4.8	7.9
	<b>562.5</b>	20	28.7	0.47	99.7	3.6	5.1	1.5	5.1	8.2
	<b>587.5</b>	21	27.3	0.50	99.7	3.9	5.3	1.8	5.3	8.5
	<b>600.0</b>	22	26.7	0.51	99.7	4.0	5.5	1.9	5.5	8.6

<sup>1</sup>values are rounded-off to the nearest integer

<b>Table 4j</b> Lookup table for basins with a bed slope of 0.1%, <i>CITRUS</i>										
$Q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{iq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>Min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.22</b>	<b>337.5</b>	11	43.0	0.21	84.3	1.6	2.8	0.3	2.8	6.1
	<b>362.5</b>	12	40.8	0.22	86.2	1.8	3.1	0.3	3.1	6.2
	<b>387.5</b>	13	38.6	0.23	88.4	2.0	3.3	0.2	3.3	6.3
	<b>412.5</b>	14	37.2	0.28	92.0	2.3	3.6	0.3	3.6	6.6
	<b>437.5</b>	15	35.5	0.32	94.1	2.5	3.9	0.6	3.9	6.9
	<b>462.5</b>	16	33.9	0.35	96.0	2.7	4.1	0.6	4.1	7.2
	<b>487.5</b>	17	32.5	0.39	98.0	3.0	4.4	0.8	4.4	7.5
	<b>512.5</b>	18	31.2	0.42	99.1	3.2	4.6	1.1	4.6	7.7
	<b>537.5</b>	19	29.6	0.45	99.5	3.4	4.9	1.3	4.9	8.0
	<b>562.5</b>	20	28.1	0.48	99.8	3.7	5.2	1.6	5.2	8.3
	<b>587.5</b>	21	26.7	0.51	99.8	4.0	5.5	1.9	5.5	8.6
<b>600.0</b>	22	26.2	0.52	100.0	4.1	5.6	2.0	5.6	8.7	
<b>0.23</b>	<b>337.5</b>	11	42.5	0.22	85.0	1.6	2.9	0.4	2.9	6.3
	<b>362.5</b>	12	40.3	0.22	86.9	1.8	3.1	0.3	3.1	6.3
	<b>387.5</b>	13	38.1	0.24	89.1	2.1	3.4	0.3	3.4	6.4
	<b>412.5</b>	14	36.5	0.28	92.1	2.3	3.7	0.2	3.7	6.7
	<b>437.5</b>	15	35.0	0.33	94.7	2.5	3.9	0.5	3.9	7.0
	<b>462.5</b>	16	33.5	0.37	96.9	2.8	4.2	0.7	4.2	7.3
	<b>487.5</b>	17	32.0	0.40	98.6	3.0	4.5	0.9	4.5	7.6
	<b>512.5</b>	18	30.6	0.43	99.2	3.3	4.7	1.2	4.7	7.9
	<b>537.5</b>	19	29.1	0.46	99.9	3.5	5.0	1.4	5.0	8.1
	<b>562.5</b>	20	27.5	0.49	99.7	3.8	5.3	1.7	5.3	8.4
	<b>587.5</b>	21	26.2	0.52	99.9	4.1	5.6	2.0	5.6	8.7
<b>600.0</b>	22	25.6	0.53	99.9	4.2	5.7	2.1	5.7	8.8	

<sup>1</sup>values are rounded-off to the nearest integer

<b>Table 4k</b> Lookup table for basins with a bed slope of 0.1%, <i>CITRUS</i>										
$Q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	-	<i>min</i>	%	%	%	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.24</b>	<b>337.5</b>	10	42.3	0.23	86.3	1.7	3.0	0.5	3.0	6.4
	<b>362.5</b>	11	39.9	0.23	87.7	1.9	3.2	0.4	3.2	6.5
	<b>387.5</b>	12	37.7	0.26	90.0	2.1	3.5	0.3	3.5	6.5
	<b>412.5</b>	13	35.9	0.29	92.4	2.4	3.7	0.3	3.7	6.8
	<b>437.5</b>	14	34.5	0.34	95.2	2.6	4.0	0.5	4.0	7.1
	<b>462.5</b>	15	33.0	0.38	97.4	2.9	4.3	0.7	4.3	7.4
	<b>487.5</b>	16	31.5	0.42	99.0	3.1	4.6	1.0	4.6	7.7
	<b>512.5</b>	17	30.1	0.44	99.6	3.4	4.8	1.2	4.8	8.0
	<b>537.5</b>	18	28.5	0.47	99.8	3.6	5.1	1.5	5.1	8.2
	<b>562.5</b>	19	27.0	0.50	99.9	3.9	5.4	1.8	5.4	8.5
	<b>600.0</b>	20	2.5	0.54	100.0	4.3	5.8	2.2	5.8	9.0
<b>0.25</b>	<b>337.5</b>	10	41.2	0.21	85.7	1.8	3.0	0.2	3.0	6.6
	<b>362.5</b>	11	39.7	0.24	88.9	2.0	3.3	0.5	3.3	6.6
	<b>387.5</b>	12	37.3	0.26	90.7	2.2	3.5	0.4	3.5	6.7
	<b>412.5</b>	13	35.6	0.30	93.3	2.4	3.8	0.3	3.8	6.9
	<b>437.5</b>	14	34.1	0.35	95.9	2.7	4.1	0.5	4.1	7.2
	<b>462.5</b>	15	32.6	0.39	98.0	2.9	4.4	0.8	4.4	7.5
	<b>487.5</b>	16	31.0	0.43	99.2	3.2	4.7	1.1	4.7	7.8
	<b>512.5</b>	17	29.6	0.45	99.8	3.5	4.9	1.3	4.9	8.1
	<b>537.5</b>	18	28.0	0.48	99.9	3.7	5.2	1.6	5.2	8.4
	<b>562.5</b>	19	26.5	0.51	99.9	4.0	5.5	1.9	5.5	8.7
		<b>587.5</b>	20	25.2	0.54	99.9	4.3	5.8	2.2	5.8
	<b>600.0</b>	21	24.6	0.55	99.9	4.5	5.9	2.3	5.9	9.1

<sup>1</sup>values are rounded-off to the nearest integer

Table 5. Coefficients and exponents of the power-law advance function

Unit inlet flow rate (cfs/s)	Citrus basins				Alfalfa basins	
	Level basin		0.1% slope		Level basin	
	$\alpha$ (min/ft $^\beta$ )*	$\beta$ (-)*	$\alpha$ (min/ft $^\beta$ )*	$\beta$ (-)*	$\alpha$ (min/ft $^\beta$ )*	$\beta$ (-)*
0.04	0.0231	1.2502	0.0382	1.1339	0.034285	1.2467
0.05	0.0204	1.2474	0.0318	1.1429	0.029765	1.2474
0.06	0.0183	1.2465	0.0143	1.2465	0.024541	1.2606
0.07	0.0217	1.2045	0.0251	1.1509	0.024814	1.2443
0.08	0.0155	1.2448	0.0222	1.1594	0.023367	1.2406
0.09	0.0144	1.2449	0.0204	1.1625	0.019324	1.2596
0.10	0.0133	1.2474	0.0204	1.1537	0.020706	1.2393
0.11	0.0126	1.2472	0.0178	1.1672	0.019679	1.2379
0.12	0.0119	1.2472	0.0163	1.1739	0.01535	1.2699
0.13	0.0114	1.2470	0.0154	1.1761	0.016862	1.2476
0.14	0.0107	1.2505	0.0146	1.1778	0.015725	1.2518
0.15	0.0101	1.2532	0.0139	1.1798	0.01374	1.2674
0.16	0.0099	1.2503	0.0133	1.1809	0.012095	1.2819
0.17	0.0095	1.2501	0.0128	1.1826	0.014565	1.2469
0.18	0.0092	1.2504	0.0123	1.1836	0.014585	1.2424
0.19	0.0089	1.2500	0.0118	1.1854	0.011839	1.2699
0.20	0.0088	1.2475	0.0110	1.1925	0.010673	1.282
0.21	0.0086	1.2466	0.0107	1.1934	0.012073	1.2569
0.22	0.0084	1.2468	0.0104	1.1944	0.010571	1.2749
0.23	0.0081	1.2474	0.0100	1.1960	0.010359	1.2743
0.24	0.0079	1.2476	0.0099	1.1942	0.010597	1.2654
0.25	0.0078	1.2470	0.0095	1.1968	0.013354	1.2254

\*  $\alpha$  and  $\beta$  are parameters of the power-law advance function:  $t_{co} = t_a = \alpha L_{co}^\beta$

$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
cfs/ft	ft	min	%	%	%	in	in	in	in	in
<b>0.04</b>	<b>362.5</b>	36	84.6	0.97	100	0.2	1.7	1.60	1.68	3.8
	<b>387.5</b>	40	77.6	0.97	100	0.4	1.8	1.75	1.85	3.8
	<b>412.5</b>	43	71.6	0.98	100	0.5	2.0	2.00	2.05	3.8
	<b>437.5</b>	46	66.5	0.98	100	0.7	2.1	2.10	2.25	3.8
	<b>462.5</b>	50	61.9	0.98	100	0.9	2.3	2.30	2.42	3.8
	<b>487.5</b>	53	57.9	0.98	100	1.0	2.4	2.50	2.51	3.8
	<b>512.5</b>	56	54.7	0.98	100	1.2	2.6	2.60	2.72	3.8
	<b>537.5</b>	60	51.5	0.98	100	1.3	2.8	2.80	2.90	3.8

	<b>562.5</b>	64	48.5	0.98	100	1.5	2.9	3.00	3.15	3.8
	<b>587.5</b>	67	45.8	0.98	100	1.7	3.1	3.20	3.23	3.8
	<b>600.0</b>	68	44.9	0.98	100	1.8	3.2	3.20	3.25	3.8
<b>0.05</b>	<b>362.5</b>	32	78.0	0.98	100	0.4	1.8	1.8	1.85	4.2
	<b>387.5</b>	34	71.6	0.98	100	0.5	2.0	2.0	2.12	4.2
	<b>412.5</b>	37	66.0	0.98	100	0.7	2.2	2.1	2.28	4.2
	<b>437.5</b>	40	61.3	0.98	100	0.9	2.4	2.3	2.45	4.2
	<b>462.5</b>	43	57.1	0.98	100	1.1	2.5	2.5	2.61	4.2
	<b>487.5</b>	46	53.4	0.98	100	1.2	2.7	2.7	2.80	4.2
	<b>512.5</b>	49	50.5	0.98	100	1.4	2.9	2.8	2.95	4.2
	<b>537.5</b>	52	47.5	0.99	100	1.6	3.1	3.0	3.14	4.2
	<b>562.5</b>	55	44.8	0.99	100	1.8	3.2	3.2	3.25	4.2
	<b>587.5</b>	58	42.4	0.99	100	2.0	3.4	3.4	3.50	4.2
	<b>600.0</b>	59	41.4	0.99	100	2.0	3.5	3.5	3.60	4.2

<sup>1</sup>values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $Du_{lq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

<b>Table 2b</b> Lookup table for level basins, <i>CITRUS</i>										
$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.06</b>	<b>362.5</b>	28	72.8	0.98	100	0.5	2.0	1.9	2.05	4.6
	<b>387.5</b>	31	66.8	0.98	100	0.7	2.2	2.1	2.25	4.6
	<b>412.5</b>	33	61.6	0.98	100	0.9	2.3	2.3	2.41	4.6
	<b>437.5</b>	36	57.2	0.98	100	1.1	2.5	2.5	2.60	4.6
	<b>462.5</b>	38	53.3	0.99	100	1.2	2.7	2.7	2.75	4.6
	<b>487.5</b>	41	49.8	0.99	100	1.4	2.9	2.9	3.00	4.6
	<b>512.5</b>	43	47.2	0.99	100	1.6	3.0	3.0	3.17	4.6
	<b>537.5</b>	46	44.3	0.99	100	1.8	3.3	3.2	3.37	4.6
	<b>562.5</b>	49	41.8	0.99	100	2.0	3.5	3.4	3.47	4.6
	<b>587.5</b>	52	39.6	0.99	100	2.2	3.7	3.6	3.77	4.6
	<b>600.0</b>	53	38.7	0.99	100	2.3	3.8	3.7	3.82	4.6
<b>0.07</b>	<b>362.5</b>	26	68.60	0.98	100	0.6	2.1	2.1	2.18	4.9
	<b>387.5</b>	28	63.00	0.98	100	0.8	2.3	2.3	2.36	4.9
	<b>412.5</b>	30	58.11	0.98	100	1.0	2.5	2.4	2.56	4.9
	<b>437.5</b>	33	53.99	0.99	100	1.2	2.7	2.6	2.76	4.9
	<b>462.5</b>	35	50.22	0.99	100	1.4	2.9	2.9	2.98	4.9
	<b>487.5</b>	37	47.00	0.99	100	1.6	3.1	3.1	3.18	4.9
	<b>512.5</b>	39	44.50	0.99	100	1.8	3.3	3.2	3.27	4.9
	<b>537.5</b>	42	41.80	0.99	100	2.0	3.5	3.4	3.47	4.9
	<b>562.5</b>	45	39.40	0.99	100	2.2	3.7	3.7	3.77	4.9
	<b>587.5</b>	47	37.30	0.99	100	2.4	3.9	3.9	3.98	4.9
	<b>600.0</b>	48	36.50	0.99	100	2.5	4.0	4.0	4.08	4.9

<sup>1</sup>values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $Du_{lq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

<b>Table 2c</b> Lookup table for level basins, <i>CITRUS</i>										
$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
cfs/ft	ft	min	%	%	%	in	in	in	in	in
<b>0.08</b>	<b>362.5</b>	24	65.1	0.98	100	0.7	2.2	2.2	2.30	5.3
	<b>387.5</b>	26	59.8	0.99	100	0.9	2.4	2.4	2.50	5.3
	<b>412.5</b>	28	55.2	0.99	100	1.1	2.6	2.6	2.70	5.3
	<b>437.5</b>	30	51.2	0.99	100	1.4	2.8	2.8	2.90	5.3
	<b>462.5</b>	32	47.7	0.99	100	1.6	3.0	3.0	3.10	5.3
	<b>487.5</b>	34	44.6	0.99	100	1.8	3.3	3.2	3.16	5.3
	<b>512.5</b>	36	42.2	0.99	100	2.0	3.4	3.4	3.50	5.3
	<b>537.5</b>	39	39.7	0.99	100	2.2	3.7	3.6	3.73	5.3
	<b>562.5</b>	41	37.4	0.99	100	2.4	3.9	3.9	3.95	5.3
	<b>587.5</b>	43	35.4	0.99	100	2.6	4.1	4.1	4.10	5.3
<b>600.0</b>	44	34.6	0.99	100	2.7	4.2	4.2	4.20	5.3	
<b>0.09</b>	<b>362.5</b>	22	62.20	0.98	100	0.8	2.3	2.3	2.40	5.6
	<b>387.5</b>	24	54.10	0.99	100	1.1	2.5	2.5	2.60	5.6
	<b>412.5</b>	26	52.60	0.99	100	1.3	2.7	2.7	2.82	5.6
	<b>437.5</b>	28	48.90	0.99	100	1.5	2.9	2.9	3.05	5.6
	<b>462.5</b>	30	45.50	0.99	100	1.7	3.2	3.2	3.25	5.6
	<b>487.5</b>	32	42.60	0.99	100	1.9	3.4	3.4	3.50	5.6
	<b>512.5</b>	34	41.75	0.99	100	2.1	3.6	3.6	3.70	5.6
	<b>537.5</b>	36	37.90	0.99	100	2.4	3.8	3.8	3.90	5.6
	<b>562.5</b>	38	35.70	0.99	100	2.6	4.1	4.1	4.15	5.6
	<b>587.5</b>	40	33.80	0.99	100	2.8	4.3	4.3	4.40	5.6
<b>600.0</b>	41	33.10	0.99	100	2.9	4.4	4.4	4.50	5.6	

<sup>1</sup>values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $Du_{lq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

<b>Table 2d</b> Lookup table for level basins, <i>CITRUS</i>										
$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.10</b>	<b>362.5</b>	21	59.6	0.99	100	0.9	2.4	2.4	2.50	5.8
	<b>387.5</b>	22	54.7	0.99	100	1.2	2.6	2.6	2.61	5.8
	<b>412.5</b>	24	50.5	0.99	100	1.4	2.9	2.8	2.92	5.8
	<b>437.5</b>	26	46.9	0.99	100	1.6	3.1	3.1	3.19	5.8
	<b>462.5</b>	28	43.7	0.99	100	1.9	3.3	3.3	3.40	5.8
	<b>487.5</b>	30	40.8	0.99	100	2.1	3.6	3.5	3.62	5.8
	<b>512.5</b>	32	38.7	0.99	100	2.3	3.8	3.7	3.82	5.8
	<b>537.5</b>	34	36.3	0.99	100	2.5	4.0	4.0	4.10	5.8
	<b>562.5</b>	36	34.3	0.99	100	2.8	4.2	4.2	4.25	5.8
	<b>587.5</b>	38	32.5	0.99	100	3.0	4.5	4.5	4.58	5.8
<b>600.0</b>	39	31.7	0.99	100	3.1	4.6	4.6	4.63	5.8	
<b>0.11</b>	<b>362.5</b>	19	57.4	0.99	100	1.0	2.5	2.5	2.60	6.1
	<b>387.5</b>	21	52.7	0.99	100	1.3	2.7	2.7	2.82	6.1
	<b>412.5</b>	23	48.6	0.99	100	1.5	3.0	3.0	3.10	6.1
	<b>437.5</b>	25	45.1	0.99	100	1.7	3.2	3.2	3.30	6.1
	<b>462.5</b>	27	42.0	0.99	100	2.0	3.4	3.4	3.52	6.1
	<b>487.5</b>	28	39.3	0.99	100	2.2	3.7	3.7	3.79	6.1
	<b>512.5</b>	30	37.2	0.99	100	2.4	3.9	3.9	4.00	6.1
	<b>537.5</b>	32	35.0	0.99	100	2.7	4.2	4.1	4.22	6.1
	<b>562.5</b>	34	33.0	0.99	100	2.9	4.4	4.4	4.50	6.1
	<b>587.5</b>	36	31.2	0.99	100	3.2	4.7	4.6	4.72	6.1
<b>600.0</b>	37	30.5	0.99	100	3.3	4.8	4.8	4.90	6.1	

<sup>1</sup>values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $Du_{lq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

<b>Table 2e</b> Lookup table for level basins, <i>CITRUS</i>										
$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.12</b>	<b>362.5</b>	18	55.4	0.99	100	1.1	2.6	2.6	2.68	6.4
	<b>387.5</b>	20	50.8	0.99	100	1.4	2.9	2.8	2.92	6.4
	<b>412.5</b>	22	46.9	0.99	100	1.6	3.1	3.1	3.18	6.4
	<b>437.5</b>	24	43.6	0.99	100	1.9	3.3	3.3	3.41	6.4
	<b>462.5</b>	25	40.6	0.99	100	2.1	3.6	3.6	3.65	6.4
	<b>487.5</b>	27	37.9	0.99	100	2.4	3.8	3.8	3.90	6.4
	<b>512.5</b>	29	35.9	0.99	100	2.6	4.1	4.0	4.10	6.4
	<b>537.5</b>	30	33.8	0.99	100	2.8	4.3	4.3	4.40	6.4
	<b>562.5</b>	32	31.9	0.99	100	3.1	4.6	4.6	4.62	6.4
	<b>587.5</b>	34	30.2	0.99	100	3.4	4.8	4.8	4.90	6.4
<b>600.0</b>	35	29.5	0.99	100	3.5	4.9	4.9	5.04	6.4	
<b>0.13</b>	<b>362.5</b>	18	53.6	0.99	100	1.2	2.7	2.7	2.77	6.6
	<b>387.5</b>	19	49.2	0.99	100	1.5	2.9	2.9	3.01	6.6
	<b>412.5</b>	21	45.4	0.99	100	1.7	3.2	3.2	3.22	6.6
	<b>437.5</b>	22	42.2	0.99	100	2.0	3.4	3.4	3.50	6.6
	<b>462.5</b>	24	39.3	0.99	100	2.2	3.7	3.7	3.78	6.6
	<b>487.5</b>	26	36.7	0.99	100	2.5	4.0	3.9	4.23	6.6
	<b>512.5</b>	27	34.8	0.99	100	2.7	4.2	4.2	4.27	6.6
	<b>537.5</b>	29	32.7	0.99	100	3.0	4.5	4.4	4.52	6.6
	<b>562.5</b>	31	30.8	0.99	100	3.3	4.7	4.7	4.80	6.6
	<b>587.5</b>	32	29.2	0.99	100	3.5	5.0	5.0	5.09	6.6
<b>600.0</b>	33	28.5	0.99	100	3.6	5.1	5.1	5.20	6.6	

<sup>1</sup>values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $Du_{lq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

<b>Table 2f</b> Lookup table for level basins, <i>CITRUS</i>										
$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.14</b>	<b>362.5</b>	17	52.0	0.99	100	1.3	2.8	2.8	2.85	6.8
	<b>387.5</b>	18	47.7	0.99	100	1.6	3.0	3.0	3.10	6.8
	<b>412.5</b>	20	44.0	0.99	100	1.8	3.3	3.3	3.38	6.8
	<b>437.5</b>	21	40.9	0.99	100	2.1	3.6	3.5	3.61	6.8
	<b>462.5</b>	23	38.1	0.99	100	2.3	3.8	3.8	3.90	6.8
	<b>487.5</b>	25	35.6	0.99	100	2.6	4.1	4.1	4.18	6.8
	<b>512.5</b>	26	33.7	0.99	100	2.8	4.3	4.3	4.40	6.8
	<b>537.5</b>	38	31.7	0.99	100	3.1	4.6	4.6	4.70	6.8
	<b>562.5</b>	29	29.9	0.99	100	3.4	4.9	4.9	4.96	6.8
	<b>587.5</b>	31	28.3	0.99	100	3.7	5.2	5.1	5.22	6.8
<b>600.0</b>	32	27.7	0.99	100	3.8	5.3	5.3	5.33	6.8	
<b>0.15</b>	<b>362.5</b>	16	50.6	0.99	100	1.4	2.9	2.8	2.93	7.1
	<b>387.5</b>	18	46.4	0.99	100	1.7	3.1	3.1	3.20	7.1
	<b>412.5</b>	19	42.8	0.99	100	1.9	3.4	3.4	3.44	7.1
	<b>437.5</b>	21	39.8	0.99	100	2.2	3.7	3.6	3.73	7.1
	<b>462.5</b>	23	37.0	0.99	100	2.5	3.9	3.9	4.00	7.1
	<b>487.5</b>	24	34.6	0.99	100	2.7	4.2	4.2	4.28	7.1
	<b>512.5</b>	25	32.8	0.99	100	3.0	4.4	4.4	4.50	7.1
	<b>537.5</b>	27	30.8	0.99	100	3.3	4.7	4.7	4.80	7.1
	<b>562.5</b>	28	29.1	0.99	100	3.5	5.0	5.0	5.18	7.1
	<b>587.5</b>	30	27.5	0.99	100	3.8	5.3	5.3	5.38	7.1
	<b>600.0</b>	30	26.9	0.99	100	3.9	5.4	5.4	5.50	7.1

<sup>1</sup>values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $Du_{lq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

<b>Table 2g</b> Lookup table for level basins, <i>CITRUS</i>										
$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.16</b>	<b>362.5</b>	16	49.2	0.99	100	1.5	2.9	2.9	3.01	7.3
	<b>387.5</b>	17	45.2	0.99	100	1.7	3.2	3.2	3.30	7.3
	<b>412.5</b>	18	41.7	0.99	100	2.0	3.5	3.5	3.55	7.3
	<b>437.5</b>	20	38.7	0.99	100	2.3	3.8	3.7	3.82	7.3
	<b>462.5</b>	21	36.1	0.99	100	2.6	4.0	4.0	4.10	7.3
	<b>487.5</b>	23	33.7	0.99	100	2.8	4.3	4.3	4.40	7.3
	<b>512.5</b>	24	31.9	0.99	100	3.1	4.6	4.5	4.62	7.3
	<b>537.5</b>	26	30.0	0.99	100	3.4	4.9	4.8	4.94	7.3
	<b>562.5</b>	27	28.3	0.99	100	3.7	5.2	5.1	5.21	7.3
	<b>587.5</b>	28	26.8	0.99	100	4.0	5.4	5.4	5.50	7.3
<b>600.0</b>	29	26.2	0.99	100	4.1	5.6	5.6	5.62	7.3	
<b>0.17</b>	<b>337.5</b>	14	51.9	0.99	100	1.3	2.8	2.8	2.85	7.5
	<b>362.5</b>	15	48.0	0.99	100	1.5	3.0	3.0	3.10	7.5
	<b>387.5</b>	16	44.1	0.99	100	1.8	3.3	3.3	3.37	7.5
	<b>412.5</b>	18	40.7	0.99	100	2.1	3.6	3.6	3.62	7.5
	<b>437.5</b>	19	37.8	0.99	100	2.4	3.9	3.8	3.92	7.5
	<b>462.5</b>	21	35.2	0.99	100	2.7	4.1	4.1	4.20	7.5
	<b>487.5</b>	22	32.9	0.99	100	3.0	4.4	4.4	4.50	7.5
	<b>512.5</b>	23	31.1	0.99	100	3.2	4.7	4.7	4.75	7.5
	<b>537.5</b>	25	29.3	0.99	100	3.5	5.0	5.0	5.02	7.5
	<b>562.5</b>	26	27.6	0.99	100	3.8	5.3	5.3	5.37	7.5
	<b>587.5</b>	27	26.2	0.99	100	4.1	5.6	5.6	5.62	7.5
<b>600.0</b>	28	25.5	0.99	100	4.2	5.7	5.7	5.80	7.5	

<sup>1</sup>values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $Du_{lq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
	<b>362.5</b>	15	46.9	0.99	100	1.6	3.1	3.1	3.16	7.7
	<b>387.5</b>	16	43.0	0.99	100	1.9	3.4	3.4	3.42	7.7
	<b>412.5</b>	17	39.7	0.99	100	2.2	3.7	3.6	3.72	7.7
	<b>437.5</b>	18	37.3	0.99	100	2.4	3.9	3.9	3.98	7.7
	<b>462.5</b>	20	34.3	0.99	100	2.8	4.2	4.2	4.30	7.7
	<b>487.5</b>	21	32.1	0.99	100	3.1	4.5	4.5	4.60	7.7
	<b>512.5</b>	22	30.4	0.99	100	3.3	4.8	4.8	4.82	7.7
	<b>537.5</b>	24	28.6	0.99	100	3.6	5.1	5.1	5.18	7.7
	<b>562.5</b>	25	27.0	0.99	100	3.9	5.4	5.4	5.50	7.7
	<b>587.5</b>	27	25.5	0.99	100	4.2	5.7	5.7	5.80	7.7
	<b>600.0</b>	27	24.9	0.99	100	4.4	5.9	5.8	5.94	7.7
	<b>362.5</b>	14	45.8	0.99	100	1.7	3.2	3.2	3.22	7.9
	<b>387.5</b>	15	42.1	0.99	100	2.0	3.5	3.4	3.52	7.9
	<b>412.5</b>	17	38.8	0.99	100	2.3	3.7	3.7	3.80	7.9
	<b>437.5</b>	18	36.0	0.99	100	2.6	4.0	4.0	4.10	7.9
	<b>462.5</b>	19	33.6	0.99	100	2.9	4.3	4.3	4.40	7.9
	<b>487.5</b>	21	31.4	0.99	100	3.2	4.6	4.6	4.70	7.9
	<b>512.5</b>	22	29.7	0.99	100	3.4	4.9	4.9	5.00	7.9
	<b>537.5</b>	23	28.0	0.99	100	3.7	5.2	5.2	5.25	7.9
	<b>562.5</b>	25	26.4	0.99	100	4.1	5.5	5.5	5.50	7.9
	<b>587.5</b>	26	25.0	0.99	100	4.4	5.9	5.8	5.95	7.9
	<b>600.0</b>	26	24.4	0.99	100	4.5	6.0	6.0	6.20	7.9

<sup>1</sup>values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $Du_{lq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

<b>Table 2i</b> Lookup table for level basins, <i>CITRUS</i>										
$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
cfs/ft	ft	min	%	%	%	in	in	in	in	in
<b>0.20</b>	<b>362.5</b>	14	44.9	0.99	100	1.8	3.2	3.2	3.30	8.1
	<b>387.5</b>	15	41.2	0.99	100	2.1	3.5	3.5	3.60	8.1
	<b>412.5</b>	16	38.0	0.99	100	2.4	3.8	3.8	3.90	8.1
	<b>437.5</b>	17	35.3	0.99	100	2.7	4.1	4.1	4.20	8.1
	<b>462.5</b>	19	32.9	0.99	100	3.0	4.4	4.4	4.50	8.1
	<b>487.5</b>	20	30.7	0.99	100	3.3	4.7	4.7	4.80	8.1
	<b>512.5</b>	21	29.1	0.99	100	3.5	5.0	5.0	5.08	8.1
	<b>537.5</b>	22	27.4	0.99	100	3.9	5.3	5.3	5.40	8.1
	<b>562.5</b>	24	25.8	0.99	100	4.2	5.7	5.6	5.80	8.1
	<b>587.5</b>	25	24.4	0.99	100	4.5	6.0	6.0	6.03	8.1
<b>600.0</b>	26	23.9	0.99	100	4.6	6.1	6.1	6.15	8.1	
<b>0.21</b>	<b>362.5</b>	13	44.0	0.99	100	1.8	3.3	3.3	3.38	8.2
	<b>387.5</b>	15	40.3	0.99	100	2.1	3.6	3.6	3.63	8.2
	<b>412.5</b>	16	37.2	0.99	100	2.4	3.9	3.9	3.97	8.2
	<b>437.5</b>	17	34.6	0.99	100	2.7	4.2	4.2	4.23	8.2
	<b>462.5</b>	18	32.2	0.99	100	3.1	4.5	4.5	4.60	8.2
	<b>487.5</b>	19	30.1	0.99	100	3.4	4.8	4.8	4.90	8.2
	<b>512.5</b>	21	28.5	0.99	100	3.6	5.1	5.1	5.20	8.2
	<b>537.5</b>	22	26.8	0.99	100	4.0	5.4	5.4	5.50	8.2
	<b>562.5</b>	23	25.3	0.99	100	4.3	5.8	5.8	5.85	8.2
	<b>587.5</b>	24	23.9	0.99	100	4.6	6.1	6.1	6.15	8.2
<b>600.0</b>	25	23.4	0.99	100	4.8	6.2	6.2	6.22	8.2	

values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $Du_{lq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

<b>Table 2j</b> Lookup table for level basins, <i>CITRUS</i>										
$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.22</b>	<b>362.5</b>	13	43.1	0.99	100	1.9	3.4	3.3	3.42	8.4
	<b>387.5</b>	14	39.6	0.99	100	2.2	3.7	3.7	3.72	8.4
	<b>412.5</b>	15	36.5	0.99	100	2.5	4.0	4.0	4.02	8.4
	<b>437.5</b>	16	33.9	0.99	100	2.8	4.3	4.3	4.38	8.4
	<b>462.5</b>	18	31.6	0.99	100	3.1	4.6	4.6	4.70	8.4
	<b>487.5</b>	19	29.5	0.99	100	3.5	4.9	4.9	5.00	8.4
	<b>512.5</b>	20	27.9	0.99	100	3.7	5.2	5.2	5.30	8.4
	<b>537.5</b>	21	26.3	0.99	100	4.1	5.6	5.5	5.61	8.4
	<b>562.5</b>	23	24.8	0.99	100	4.4	5.9	5.9	5.97	8.4
	<b>587.5</b>	24	23.5	0.99	100	4.7	6.2	6.2	6.30	8.4
<b>600.0</b>	25	22.9	0.99	100	4.9	6.4	6.4	6.18	8.4	
<b>0.23</b>	<b>362.5</b>	13	42.3	0.99	100	2.0	3.4	3.4	3.50	8.6
	<b>387.5</b>	14	38.8	0.99	100	2.3	3.7	3.7	3.80	8.6
	<b>412.5</b>	15	35.8	0.99	100	2.6	4.1	4.0	4.15	8.6
	<b>437.5</b>	16	33.3	0.99	100	2.9	4.4	4.4	4.44	8.6
	<b>462.5</b>	17	31.0	0.99	100	3.2	4.7	4.7	4.78	8.6
	<b>487.5</b>	18	29.0	0.99	100	3.6	5.0	5.0	5.10	8.6
	<b>512.5</b>	19	27.4	0.99	100	3.8	5.3	5.3	5.40	8.6
	<b>537.5</b>	20	25.8	0.99	100	4.2	5.7	5.6	5.80	8.6
	<b>562.5</b>	22	24.3	0.99	100	4.5	6.0	6.0	6.03	8.6
	<b>587.5</b>	23	23.0	0.99	100	4.9	6.3	6.3	6.30	8.6
<b>600.0</b>	24	22.5	0.99	100	5.0	6.5	6.5	6.52	8.6	

<sup>1</sup>values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $Du_{lq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
cfs/ft	ft	min	%	%	%	in	in	in	in	in
<b>0.24</b>	<b>362.5</b>	12	41.5	0.99	100	2.0	3.5	3.5	3.48	8.8
	<b>387.5</b>	13	38.1	0.99	100	2.3	3.8	3.8	3.90	8.8
	<b>412.5</b>	15	35.2	0.99	100	2.7	4.1	4.1	4.20	8.8
	<b>437.5</b>	16	32.7	0.99	100	3.0	4.5	4.4	4.55	8.8
	<b>462.5</b>	17	30.4	0.99	100	3.3	4.8	4.8	4.84	8.8
	<b>487.5</b>	18	28.5	0.99	100	3.7	5.1	5.1	5.20	8.8
	<b>512.5</b>	19	26.9	0.99	100	3.9	5.4	5.4	5.50	8.8
	<b>537.5</b>	20	25.3	0.99	100	4.3	5.8	5.7	5.90	8.8
	<b>562.5</b>	21	23.9	0.99	100	4.6	6.1	6.1	6.15	8.8
	<b>587.5</b>	23	22.6	0.99	100	5.0	6.5	6.4	6.50	8.8
<b>600.0</b>	24	22.1	0.99	100	5.1	6.6	6.6	6.70	8.8	
<b>0.25</b>	<b>362.5</b>	12	40.8	0.99	100	2.1	3.6	3.5	3.61	8.9
	<b>387.5</b>	13	37.5	0.99	100	2.4	3.9	3.9	3.95	8.9
	<b>412.5</b>	14	34.6	0.99	100	2.7	4.2	4.2	4.30	8.9
	<b>437.5</b>	15	32.1	0.99	100	3.1	4.5	4.5	4.60	8.9
	<b>462.5</b>	16	29.9	0.99	100	3.4	4.9	4.9	4.95	8.9
	<b>487.5</b>	18	28.0	0.99	100	3.7	5.2	5.2	5.25	8.9
	<b>512.5</b>	19	26.5	0.99	100	4.0	5.5	5.5	5.60	8.9
	<b>537.5</b>	20	24.9	0.99	100	4.4	5.9	5.9	5.97	8.9
	<b>562.5</b>	21	23.5	0.99	100	4.7	6.2	6.2	6.25	8.9
	<b>587.5</b>	22	22.2	0.99	100	5.1	6.6	6.6	6.60	8.9
<b>600.0</b>	23	21.7	0.99	100	5.3	6.7	6.7	6.75	8.9	

values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $Du_{lq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.04</b>	<b>337.5</b>	49	63.0	0.97	100	0.8	2.3	2.2	2.3	5.1
	<b>362.5</b>	53	58.2	0.97	100	1.0	2.5	2.4	2.5	5.2
	<b>387.5</b>	58	53.4	0.97	100	1.2	2.7	2.6	2.7	5.3
	<b>412.5</b>	62	49.2	0.98	100	1.5	2.9	2.9	2.9	5.4
	<b>437.5</b>	67	45.7	0.98	100	1.7	3.2	3.1	3.2	5.4
	<b>462.5</b>	72	42.6	0.98	100	1.9	3.4	3.3	3.4	5.5
	<b>487.5</b>	77	39.8	0.98	100	2.2	3.7	3.6	3.7	5.6
	<b>512.5</b>	82	37.6	0.98	100	2.4	3.9	3.8	3.9	5.6
	<b>537.5</b>	87	35.4	0.98	100	2.6	4.1	4.0	4.1	5.7
	<b>562.5</b>	92	33.3	0.98	100	2.9	4.4	4.3	4.4	5.7
	<b>587.5</b>	97	31.6	0.98	100	3.1	4.6	4.5	4.6	5.8
	<b>600.0</b>	100	30.8	0.98	100	3.3	4.7	4.7	4.7	5.8
<b>0.05</b>	<b>337.5</b>	43	57.8	0.97	100	1.0	2.5	2.4	2.5	5.7
	<b>362.5</b>	46	53.4	0.98	100	1.2	2.7	2.6	2.7	5.8
	<b>387.5</b>	50	49.0	0.98	100	1.5	3.0	2.9	3.0	5.9
	<b>412.5</b>	54	45.2	0.98	100	1.7	3.2	3.1	3.2	5.9
	<b>437.5</b>	59	41.9	0.98	100	2.0	3.5	3.4	3.5	6.0
	<b>462.5</b>	63	39.0	0.98	100	2.3	3.7	3.7	3.7	6.1
	<b>487.5</b>	67	36.5	0.98	100	2.5	3.9	3.9	3.9	6.2
	<b>512.5</b>	71	34.5	0.98	100	2.7	4.2	4.2	4.2	6.2
	<b>537.5</b>	76	32.5	0.98	100	3.0	4.5	4.4	4.5	6.3
	<b>562.5</b>	80	30.6	0.99	100	3.3	4.8	4.7	4.8	6.4
	<b>587.5</b>	85	29.0	0.99	100	3.6	5.0	5.0	5.0	6.4
	<b>600.0</b>	87	28.3	0.99	100	3.7	5.2	5.1	5.2	6.5

<sup>1</sup>values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $Du_{lq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

<b>Table 3b</b> Lookup table for level basin, <i>ALFALFA</i>										
$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.06</b>	<b>337.5</b>	38	53.8	0.98	100	1.2	2.7	2.6	2.7	6.2
	<b>362.5</b>	41	49.7	0.98	100	1.4	2.9	2.8	2.9	6.3
	<b>387.5</b>	45	45.6	0.98	100	1.7	3.2	3.1	3.2	6.4
	<b>412.5</b>	49	42.0	0.98	100	2.0	3.5	3.4	3.5	6.5
	<b>437.5</b>	52	39.0	0.98	100	2.3	3.7	3.7	3.7	6.6
	<b>462.5</b>	56	36.3	0.99	100	2.5	4.0	3.9	4.0	6.6
	<b>487.5</b>	60	34.0	0.99	100	2.8	4.3	4.2	4.3	6.7
	<b>512.5</b>	64	32.1	0.99	100	3.1	4.5	4.5	4.5	6.8
	<b>537.5</b>	68	30.2	0.99	100	3.4	4.8	4.8	4.8	6.9
	<b>562.5</b>	72	28.5	0.99	100	3.6	5.1	5.1	5.1	6.9
	<b>587.5</b>	76	27.0	0.99	100	3.9	5.4	5.4	5.4	7.0
	<b>600</b>	78	26.3	0.99	100	4.1	5.5	5.5	5.5	7.0
<b>0.07</b>	<b>337.5</b>	35	50.5	0.98	100	1.4	2.4	2.8	2.9	6.6
	<b>362.5</b>	38	46.7	0.98	100	1.6	3.1	3.0	3.1	6.7
	<b>387.5</b>	41	42.8	0.98	100	1.9	3.4	3.3	3.4	6.8
	<b>412.5</b>	44	39.5	0.98	100	2.2	3.7	3.6	3.7	6.9
	<b>437.5</b>	48	36.7	0.99	100	2.5	4.0	3.9	4.0	7.0
	<b>462.5</b>	52	34.1	0.99	100	2.8	4.3	4.2	4.3	7.1
	<b>487.5</b>	55	31.9	0.99	100	3.1	4.6	4.5	4.6	7.2
	<b>512.5</b>	58	30.2	0.99	100	3.4	4.8	4.8	4.8	7.3
	<b>537.5</b>	62	28.4	0.99	100	3.7	5.1	5.1	5.1	7.4
	<b>562.5</b>	65	26.8	0.99	100	4.0	5.4	5.4	5.4	7.5
	<b>587.5</b>	70	25.4	0.99	100	4.5	5.8	5.7	5.8	7.5
	<b>600</b>	71	24.8	0.99	100	4.4	5.9	5.8	5.9	7.6

<sup>1</sup>values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $Du_{lq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

**Table 3c** Lookup table for level basin, *ALFALFA*

$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.08</b>	<b>337.5</b>	32	47.9	0.98	100	1.6	3.0	3.0	3.0	7.1
	<b>362.5</b>	35	44.2	0.98	100	1.8	3.3	3.2	3.3	7.2
	<b>387.5</b>	38	40.6	0.99	100	2.1	3.6	3.5	3.6	7.3
	<b>412.5</b>	41	37.4	0.99	100	2.4	3.9	3.8	3.9	7.4
	<b>437.5</b>	44	34.7	0.99	100	2.7	4.2	4.1	4.2	7.5
	<b>462.5</b>	47	32.3	0.99	100	3.0	4.5	4.5	4.5	7.6
	<b>487.5</b>	51	30.2	0.99	100	3.3	4.8	4.8	4.8	7.7
	<b>512.5</b>	54	28.6	0.99	100	3.6	5.1	5.1	5.1	7.8
	<b>537.5</b>	57	26.9	0.99	100	3.9	5.4	5.4	5.4	7.9
	<b>562.5</b>	60	25.4	0.99	100	4.3	5.8	5.7	5.8	7.9
	<b>587.5</b>	64	24.0	0.99	100	4.6	6.1	6.0	6.1	8.0
<b>600.0</b>	65	23.5	0.99	100	4.8	6.2	6.2	6.2	8.1	
<b>0.09</b>	<b>337.5</b>	30	45.6	0.98	100	1.7	3.2	3.1	3.2	7.5
	<b>362.5</b>	32	42.1	0.98	100	2.0	3.4	3.4	3.4	7.6
	<b>387.5</b>	35	38.6	0.99	100	2.3	3.8	3.7	3.8	7.7
	<b>412.5</b>	38	35.7	0.99	100	2.6	4.1	4.0	4.1	7.8
	<b>437.5</b>	41	33.1	0.99	100	2.9	4.4	4.4	4.4	7.9
	<b>462.5</b>	44	30.8	0.99	100	3.3	4.7	4.7	4.7	8.0
	<b>487.5</b>	47	28.8	0.99	100	3.6	5.1	5.0	5.1	8.1
	<b>512.5</b>	50	27.3	0.99	100	3.9	5.4	5.3	5.4	8.2
	<b>537.5</b>	53	25.6	0.99	100	4.2	5.7	5.7	5.7	8.3
	<b>562.5</b>	56	24.2	0.99	100	4.6	6.0	6.0	6.0	8.4
	<b>587.5</b>	60	22.9	0.99	100	4.9	6.4	6.3	6.4	8.5
<b>600</b>	61	22.4	0.99	100	5.1	6.5	6.5	6.5	8.5	

<sup>1</sup>values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $Du_{lq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.10</b>	<b>337.5</b>	28	43.6	0.98	100	1.9	3.3	3.3	3.3	7.8
	<b>362.5</b>	31	40.3	0.99	100	2.1	3.6	3.6	3.6	7.9
	<b>387.5</b>	33	37.0	0.99	100	2.5	3.9	3.9	3.9	8.1
	<b>412.5</b>	36	34.1	0.99	100	2.8	4.3	4.2	4.3	8.2
	<b>437.5</b>	39	31.7	0.99	100	3.1	4.6	4.6	4.6	8.3
	<b>462.5</b>	42	29.5	0.99	100	3.5	4.9	4.9	4.9	8.4
	<b>487.5</b>	45	27.6	0.99	100	3.8	5.3	5.2	5.3	8.5
	<b>512.5</b>	47	26.1	0.99	100	4.1	5.6	5.6	5.6	8.6
	<b>537.5</b>	50	24.6	0.99	100	4.5	5.9	5.9	5.9	8.7
	<b>562.5</b>	53	23.2	0.99	100	4.8	6.3	6.3	6.3	8.8
	<b>587.5</b>	56	21.9	0.99	100	5.2	6.7	6.6	6.7	8.9
<b>600.0</b>	57	21.4	0.99	100	5.4	6.8	6.8	6.8	8.9	
<b>0.11</b>	<b>337.5</b>	27	41.9	0.99	100	2.0	3.5	3.4	3.5	8.2
	<b>362.5</b>	29	38.8	0.99	100	2.3	3.8	3.7	3.7	8.3
	<b>387.5</b>	31	35.6	0.99	100	2.6	4.1	4.1	4.1	8.4
	<b>412.5</b>	34	32.8	0.99	100	3.0	4.4	4.4	4.4	8.6
	<b>437.5</b>	32	30.8	0.99	100	3.3	4.7	4.7	4.7	8.7
	<b>462.5</b>	39	28.4	0.99	100	3.7	5.1	5.1	5.1	8.8
	<b>487.5</b>	42	26.5	0.99	100	4.0	5.5	5.5	5.5	8.9
	<b>512.5</b>	45	25.1	0.99	100	4.3	5.8	5.8	5.8	9.0
	<b>537.5</b>	47	23.6	0.99	100	4.7	6.2	6.2	6.2	9.1
	<b>562.5</b>	50	22.3	0.99	100	5.1	6.6	6.5	6.6	9.2
	<b>587.5</b>	53	21.1	0.99	100	5.5	6.9	6.9	6.9	9.3
<b>600</b>	54	20.6	0.99	100	5.6	7.1	7.1	7.1	9.3	

<sup>1</sup>values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $Du_{lq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.12</b>	<b>337.5</b>	25	40.4	0.99	100	2.1	3.6	3.5	3.6	8.5
	<b>362.5</b>	27	37.4	0.99	100	2.4	3.9	3.8	3.9	8.6
	<b>387.5</b>	30	34.3	0.99	100	2.8	4.2	4.2	4.2	8.8
	<b>412.5</b>	32	31.6	0.99	100	3.1	4.6	4.6	4.6	8.9
	<b>437.5</b>	35	29.4	0.99	100	3.5	4.9	4.9	4.9	9.0
	<b>462.5</b>	37	27.3	0.99	100	3.9	5.3	5.3	5.3	9.2
	<b>487.5</b>	40	25.6	0.99	100	4.2	5.7	5.7	5.7	9.3
	<b>512.5</b>	42	24.2	0.99	100	4.6	6.0	6.0	6.0	9.4
	<b>537.5</b>	45	22.8	0.99	100	4.9	6.4	6.4	6.4	9.5
	<b>562.5</b>	48	21.5	0.99	100	5.3	6.8	6.8	6.8	9.6
	<b>587.5</b>	50	20.3	0.99	100	5.7	7.2	7.2	7.2	9.7
<b>600.0</b>	52	19.8	0.99	100	5.9	7.4	7.3	7.4	9.7	
<b>0.13</b>	<b>337.5</b>	24	39.1	0.99	100	2.2	3.7	3.7	3.7	8.8
	<b>362.5</b>	26	36.1	0.99	100	2.6	4.0	4.0	4.0	9.0
	<b>387.5</b>	29	33.2	0.99	100	2.9	4.4	4.4	4.4	9.1
	<b>412.5</b>	31	30.6	0.99	100	3.3	4.8	4.7	4.7	9.3
	<b>437.5</b>	33	28.4	0.99	100	3.7	5.1	5.1	5.1	9.4
	<b>462.5</b>	36	26.4	0.99	100	4.0	5.5	5.5	5.5	9.5
	<b>487.5</b>	38	24.7	0.99	100	4.4	5.9	5.9	5.9	9.6
	<b>512.5</b>	40	23.4	0.99	100	4.8	6.2	6.2	6.2	9.7
	<b>537.5</b>	43	22.0	0.99	100	5.2	6.0	6.0	6.0	9.8
	<b>562.5</b>	46	20.8	0.99	100	5.6	7.0	7.0	7.0	9.9
	<b>587.5</b>	48	19.6	0.99	100	6.0	7.4	7.4	7.4	10.0
<b>600</b>	49	19.2	0.99	100	6.1	7.6	7.6	7.6	10.1	

<sup>1</sup>values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $Du_{lq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.14</b>	<b>337.5</b>	23	37.9	0.99	100	2.4	3.8	3.8	3.8	9.1
	<b>362.5</b>	25	35.0	0.99	100	2.7	4.2	4.1	4.2	9.3
	<b>387.5</b>	27	32.1	0.99	100	3.1	4.5	4.5	4.5	9.4
	<b>412.5</b>	30	29.6	0.99	100	3.4	4.9	4.9	4.9	9.6
	<b>437.5</b>	32	27.5	0.99	100	3.8	5.3	5.3	5.3	9.7
	<b>462.5</b>	34	25.6	0.99	100	4.2	5.7	5.7	5.7	9.8
	<b>487.5</b>	37	24.0	0.99	100	4.6	6.1	6.1	6.1	10.0
	<b>512.5</b>	38	22.7	0.99	100	5.0	6.4	6.4	6.4	10.1
	<b>537.5</b>	41	21.3	0.99	100	5.4	6.9	6.8	6.9	10.2
	<b>562.5</b>	44	20.1	0.99	100	5.8	7.3	7.2	7.3	10.3
	<b>587.5</b>	46	19.0	0.99	100	6.2	7.7	7.7	7.7	10.4
<b>600</b>	47	18.6	0.99	100	6.4	7.9	7.8	7.9	10.4	
<b>0.15</b>	<b>337.5</b>	22	36.8	0.99	100	2.5	4.0	3.9	4.0	9.4
	<b>362.5</b>	24	34.0	0.99	100	2.8	4.3	4.2	4.3	9.6
	<b>387.5</b>	26	31.2	0.99	100	3.2	4.7	4.6	4.7	9.7
	<b>412.5</b>	28	28.8	0.99	100	3.6	5.0	5.0	5.1	9.9
	<b>437.5</b>	31	26.7	0.99	100	4.0	5.5	5.4	5.5	10.0
	<b>462.5</b>	33	24.9	0.99	100	4.4	5.9	5.8	5.9	10.2
	<b>487.5</b>	35	23.3	0.99	100	4.8	6.3	6.2	6.3	10.3
	<b>512.5</b>	38	22.0	0.99	100	5.2	6.6	6.6	6.6	10.4
	<b>537.5</b>	40	20.7	0.99	100	5.6	7.1	7.0	7.1	10.5
	<b>562.5</b>	42	19.5	0.99	100	6.0	7.5	7.5	7.5	10.6
	<b>587.5</b>	44	18.5	0.99	100	6.4	7.9	7.9	7.9	10.7
<b>600</b>	45	18.1	0.99	100	6.6	8.1	8.1	8.1	10.8	

<sup>1</sup>values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $Du_{lq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>In</i>
<b>0.16</b>	<b>337.5</b>	21	35.8	0.99	100	2.6	4.1	4.0	4.1	9.7
	<b>362.5</b>	23	33.1	0.99	100	2.9	4.4	4.4	4.4	9.9
	<b>387.5</b>	25	30.4	0.99	100	3.3	4.8	4.8	4.8	10.0
	<b>412.5</b>	27	28.0	0.99	100	3.7	5.2	5.2	5.2	10.2
	<b>437.5</b>	30	26.0	0.99	100	4.1	5.6	5.6	5.6	10.3
	<b>462.5</b>	32	24.2	0.99	100	4.6	6.0	6.0	6.0	10.5
	<b>487.5</b>	34	22.6	0.99	100	5.0	6.5	6.4	6.5	10.6
	<b>512.5</b>	36	21.4	0.99	100	5.3	6.8	6.8	6.8	10.7
	<b>537.5</b>	38	20.2	0.99	100	5.8	7.3	7.2	7.3	10.8
	<b>562.5</b>	40	19.0	0.99	100	6.2	7.7	7.7	7.7	10.9
	<b>587.5</b>	43	18.0	0.99	100	6.7	8.1	8.1	8.1	11.1
<b>600.0</b>	44	17.6	0.99	100	6.8	8.3	8.3	8.3	11.1	
<b>0.17</b>	<b>337.5</b>	21	34.9	0.99	100	2.7	4.2	4.1	4.2	10.0
	<b>362.5</b>	22	32.2	0.99	100	3.0	4.5	4.5	4.5	10.2
	<b>387.5</b>	24	29.6	0.99	100	3.5	4.9	4.9	4.9	10.3
	<b>412.5</b>	27	27.3	0.99	100	3.9	5.3	5.3	5.3	10.5
	<b>437.5</b>	29	25.3	0.99	100	4.3	5.8	5.7	5.8	10.6
	<b>462.5</b>	31	23.6	0.99	100	4.7	6.2	6.2	6.2	10.8
	<b>487.5</b>	33	22.1	0.99	100	5.2	6.6	6.6	6.6	10.9
	<b>512.5</b>	35	20.9	0.99	100	5.5	7.0	7.0	7.0	11.0
	<b>537.5</b>	37	19.6	0.99	100	6.0	7.4	7.4	7.4	11.1
	<b>562.5</b>	39	18.5	0.99	100	6.4	7.9	7.9	7.9	11.3
	<b>587.5</b>	41	17.5	0.99	100	6.9	8.3	8.3	8.3	11.4
<b>600.0</b>	42	17.1	0.99	100	7.1	8.5	8.5	8.5	11.4	

<sup>1</sup>values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $Du_{lq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.18</b>	<b>337.5</b>	20	34.1	0.99	100	2.8	4.3	4.2	4.3	10.3
	<b>362.5</b>	22	31.5	0.99	100	3.2	4.6	4.6	4.6	10.4
	<b>387.5</b>	24	28.9	0.99	100	3.6	5.1	5.0	5.1	10.6
	<b>412.5</b>	26	26.6	0.99	100	4.0	5.5	5.4	5.5	10.8
	<b>437.5</b>	28	24.7	0.99	100	4.4	5.9	5.9	5.9	10.9
	<b>462.5</b>	30	23.0	0.99	100	4.9	6.3	6.3	6.3	11.1
	<b>487.5</b>	32	21.5	0.99	100	5.3	6.8	6.8	6.8	11.2
	<b>512.5</b>	34	20.4	0.99	100	5.7	7.2	7.1	7.2	11.3
	<b>537.5</b>	36	19.2	0.99	100	6.2	7.6	7.6	7.6	11.4
	<b>562.5</b>	38	18.1	0.99	100	6.6	8.1	8.1	8.1	11.6
	<b>587.5</b>	40	17.1	0.99	100	7.1	8.6	8.5	8.6	11.7
<b>600.0</b>	41	16.7	0.99	100	7.3	8.8	8.7	8.8	11.7	
<b>0.19</b>	<b>337.5</b>	19	33.3	0.99	100	2.9	4.4	4.3	4.4	10.5
	<b>362.5</b>	21	30.7	0.99	100	3.3	4.7	4.7	4.7	10.7
	<b>387.5</b>	23	28.2	0.99	100	3.7	5.2	5.1	5.2	10.9
	<b>412.5</b>	25	26.0	0.99	100	4.1	5.6	5.6	5.6	11.0
	<b>437.5</b>	27	24.2	0.99	100	4.6	6.0	6.0	6.0	11.2
	<b>462.5</b>	29	22.5	0.99	100	5.0	6.5	6.5	6.5	11.3
	<b>487.5</b>	31	21.0	0.99	100	5.5	6.9	6.9	6.9	11.5
	<b>512.5</b>	32	19.9	0.99	100	5.9	7.3	7.3	7.3	11.6
	<b>537.5</b>	34	18.7	0.99	100	6.3	7.8	7.8	7.8	11.7
	<b>562.5</b>	37	17.7	0.99	100	6.8	8.3	8.3	8.3	11.9
	<b>587.5</b>	39	16.7	0.99	100	7.3	8.8	8.7	8.8	12.0
<b>600</b>	40	16.3	0.99	100	7.5	9.0	8.9	9.0	12.0	

<sup>1</sup>values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $Du_{lq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>In</i>
<b>0.20</b>	<b>337.5</b>	19	32.5	0.99	100	3.0	4.5	4.4	4.5	10.8
	<b>362.5</b>	20	30.1	0.99	100	3.4	4.9	4.8	4.9	10.9
	<b>387.5</b>	22	27.6	0.99	100	3.8	5.3	5.3	5.3	11.1
	<b>412.5</b>	24	25.5	0.99	100	4.3	5.7	5.7	5.7	11.3
	<b>437.5</b>	26	23.6	0.99	100	4.7	6.2	6.2	6.2	11.4
	<b>462.5</b>	28	22.0	0.99	100	5.2	6.6	6.6	6.6	11.6
	<b>487.5</b>	30	20.6	0.99	100	5.6	7.1	7.1	7.1	11.7
	<b>512.5</b>	32	19.5	0.99	100	6.0	7.5	7.5	7.5	11.9
	<b>537.5</b>	33	18.3	0.99	100	6.5	8.0	8.0	8.0	12.0
	<b>562.5</b>	36	17.3	0.99	100	7.0	8.5	8.4	8.5	12.1
	<b>587.5</b>	38	16.4	0.99	100	7.5	8.9	8.9	8.9	12.3
<b>600</b>	39	16.0	0.99	100	7.7	9.2	9.1	9.2	12.3	
<b>0.21</b>	<b>337.5</b>	18	31.9	0.99	100	3.1	4.6	4.5	4.6	11.0
	<b>362.5</b>	20	29.5	0.99	100	3.5	5.0	4.9	5.0	11.2
	<b>387.5</b>	22	27.0	0.99	100	3.9	5.4	5.4	5.4	11.4
	<b>412.5</b>	23	24.9	0.99	100	4.4	5.9	5.8	5.9	11.6
	<b>437.5</b>	25	23.1	0.99	100	4.8	6.3	6.3	6.3	11.7
	<b>462.5</b>	27	38.3	0.99	100	5.3	6.8	6.8	6.8	11.9
	<b>487.5</b>	29	20.2	0.99	100	5.8	7.2	7.2	7.2	12.0
	<b>512.5</b>	31	19.1	0.99	100	6.2	7.7	7.6	7.7	12.1
	<b>537.5</b>	33	17.9	0.99	100	6.7	8.2	8.1	8.2	12.3
	<b>562.5</b>	35	16.9	0.99	100	7.2	8.7	8.6	8.7	12.4
	<b>587.5</b>	36	16.0	0.99	100	7.7	9.1	9.1	9.1	12.5
<b>600</b>	37	15.6	0.99	100	7.9	9.4	9.3	9.4	12.6	

<sup>1</sup>values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $Du_{lq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>In</i>
<b>0.22</b>	<b>337.5</b>	18	31.2	0.99	100	3.2	4.7	4.6	4.7	11.3
	<b>362.5</b>	19	28.9	0.99	100	3.6	5.1	5.0	5.1	11.4
	<b>387.5</b>	21	26.5	0.99	100	4.0	5.5	5.5	5.5	11.6
	<b>412.5</b>	23	24.4	0.99	100	4.5	6.0	6.0	6.0	11.8
	<b>437.5</b>	25	22.7	0.99	100	5.0	6.4	6.4	6.4	12.0
	<b>462.5</b>	26	21.1	0.99	100	5.4	6.9	6.9	6.9	12.1
	<b>487.5</b>	28	19.8	0.99	100	5.9	7.4	7.4	7.4	12.3
	<b>512.5</b>	30	18.7	0.99	100	6.3	7.8	7.8	7.8	12.4
	<b>537.5</b>	32	17.6	0.99	100	6.8	8.3	8.3	8.3	12.5
	<b>562.5</b>	34	16.6	0.99	100	7.4	8.8	8.8	8.8	12.7
	<b>587.5</b>	36	15.7	0.99	100	7.9	9.3	9.3	9.3	12.8
<b>600.0</b>	37	15.3	0.99	100	8.1	9.5	9.5	9.5	12.9	
<b>0.23</b>	<b>337.5</b>	17	30.6	0.99	100	3.3	4.8	4.7	4.8	11.5
	<b>362.5</b>	19	28.3	0.99	100	3.7	5.1	5.1	5.1	11.7
	<b>387.5</b>	21	26.0	0.99	100	4.1	5.6	5.6	5.6	11.8
	<b>412.5</b>	22	24.0	0.99	100	4.6	6.1	6.1	6.1	12.0
	<b>437.5</b>	24	22.3	0.99	100	5.1	6.6	6.5	6.6	12.2
	<b>462.5</b>	26	20.7	0.99	100	5.6	7.1	7.0	7.1	12.4
	<b>487.5</b>	28	19.4	0.99	100	6.1	7.5	7.5	7.5	12.5
	<b>512.5</b>	29	18.3	0.99	100	6.5	8.0	8.0	8.0	12.7
	<b>537.5</b>	31	17.2	0.99	100	7.0	8.5	8.5	8.5	12.8
	<b>562.5</b>	33	16.3	0.99	100	7.5	9.0	9.0	9.0	12.9
	<b>587.5</b>	35	15.4	0.99	100	8.0	9.5	9.5	9.5	13.1
<b>600.0</b>	36	15.0	0.99	100	8.3	9.7	9.7	9.7	13.1	

<sup>1</sup>values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $Du_{lq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>In</i>	<i>in</i>	<i>in</i>
<b>0.24</b>	<b>337.5</b>	17	30.1	0.99	100	3.4	4.8	4.8	4.8	11.7
	<b>362.5</b>	18	27.8	0.99	100	3.8	5.2	5.2	5.2	11.9
	<b>387.5</b>	20	25.5	0.99	100	4.3	5.7	5.7	5.7	12.1
	<b>412.5</b>	22	23.5	0.99	100	4.7	6.2	6.2	6.2	12.3
	<b>437.5</b>	23	21.8	0.99	100	5.2	6.7	6.7	6.7	12.5
	<b>462.5</b>	25	20.3	0.99	100	5.7	7.2	7.2	7.2	12.6
	<b>487.5</b>	27	19.0	0.99	100	6.2	7.7	7.7	7.7	12.8
	<b>512.5</b>	28	18.0	0.99	100	6.7	8.8	8.1	8.1	12.9
	<b>537.5</b>	30	16.9	0.99	100	7.2	8.6	8.6	8.6	13.1
	<b>562.5</b>	32	16.0	0.99	100	7.7	9.2	9.2	9.2	13.2
	<b>587.5</b>	34	15.1	0.99	100	8.2	9.7	9.7	9.7	13.3
	<b>600.0</b>	35	14.8	0.99	100	8.4	9.9	9.9	9.9	13.4
<b>0.25</b>	<b>337.5</b>	17	29.6	0.99	100	3.5	4.9	4.9	4.9	12.0
	<b>362.5</b>	18	27.3	0.99	100	3.9	5.3	5.3	5.3	12.1
	<b>387.5</b>	20	25.1	0.99	100	4.4	5.8	5.8	5.8	12.3
	<b>412.5</b>	21	23.1	0.99	100	4.8	6.3	6.3	6.3	12.5
	<b>437.5</b>	23	21.5	0.99	100	5.3	6.8	6.8	6.8	12.7
	<b>462.5</b>	25	20.0	0.99	100	5.8	7.3	7.3	7.3	12.9
	<b>487.5</b>	26	18.7	0.99	100	6.4	7.8	7.8	7.8	13.0
	<b>512.5</b>	28	17.7	0.99	100	6.8	8.3	8.2	8.3	13.2
	<b>537.5</b>	30	16.6	0.99	100	7.3	8.8	8.8	8.8	13.3
	<b>562.5</b>	31	15.7	0.99	100	7.9	9.3	9.3	9.3	13.5
	<b>587.5</b>	33	14.9	0.99	100	8.4	9.9	9.8	9.8	13.6
	<b>600.0</b>	34	14.5	0.99	100	8.6	10.1	10.1	10.1	13.7

<sup>1</sup>values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $Du_{lq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

<b>Table 4a</b> Lookup table for basins with a bed slope of 0.1%, <i>CITRUS</i>										
$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$D_{ulq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	-	<i>min</i>	%	%	%	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.04</b>	<b>337.5</b>	28	75.0	0.51	68.9	0.3	1.3	0.6	1.3	2.9
	<b>362.5</b>	31	69.2	0.41	68.9	0.4	1.4	0.1	1.4	3.2
	<b>387.5</b>	33	66.5	0.42	71.4	0.5	1.5	0.5	1.5	3.4
	<b>412.5</b>	35	64.2	0.41	73.5	0.5	1.6	0.6	1.6	3.7
	<b>437.5</b>	38	61.0	0.39	74.6	0.6	1.7	0.5	1.8	3.9
	<b>462.5</b>	40	58.3	0.36	76.0	0.7	1.9	0.4	1.9	4.1
	<b>487.5</b>	43	56.7	0.36	78.6	0.8	2.0	0.6	2.0	4.3
	<b>512.5</b>	45	53.8	0.33	78.8	0.9	2.1	0.5	2.1	4.5
	<b>537.5</b>	48	52.2	0.32	80.7	1.0	2.2	0.6	2.2	4.7
	<b>562.5</b>	50	50.4	0.32	82.1	1.1	2.3	0.7	2.4	4.9
	<b>587.5</b>	53	48.9	0.31	83.6	1.2	2.5	0.7	2.5	5.0
<b>600.0</b>	54	48.1	0.30	84.0	1.3	2.5	0.7	2.5	5.1	
<b>0.05</b>	<b>337.5</b>	25	69.4	0.45	70.1	0.4	1.4	0.5	1.4	3.3
	<b>362.5</b>	27	64.9	0.36	71.1	0.5	1.6	0.1	1.6	3.5
	<b>387.5</b>	29	62.0	0.38	73.3	0.6	1.7	0.4	1.7	3.8
	<b>412.5</b>	31	60.3	0.38	76.1	0.7	1.8	0.6	1.8	4.0
	<b>437.5</b>	33	56.7	0.34	76.4	0.8	1.9	0.5	1.9	4.2
	<b>462.5</b>	35	54.8	0.35	78.8	0.9	2.1	0.6	2.1	4.4
	<b>487.5</b>	38	52.9	0.32	80.8	1.0	2.2	0.6	2.2	4.7
	<b>512.5</b>	40	50.1	0.29	80.9	1.1	2.3	0.5	2.3	4.9
	<b>537.5</b>	42	48.7	0.29	83.0	1.2	2.5	0.7	2.5	5.1
	<b>562.5</b>	44	46.6	0.27	83.7	1.4	2.6	0.5	2.6	5.2
	<b>587.5</b>	46	45.2	0.26	85.2	1.5	2.7	0.7	2.7	5.4
<b>600.0</b>	47	44.6	0.26	85.9	1.5	2.8	0.7	2.8	5.5	

values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $D_{ulq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

<b>Table 4b</b> Lookup table for basins with a bed slope of 0.1%, <i>CITRUS</i>										
$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
cfs/ft	-	min	%	%	%	in	in	in	in	in
<b>0.06</b>	<b>337.5</b>	22	64.7	0.36	70.7	0.5	1.6	0.1	1.6	3.5
	<b>362.5</b>	24	61.6	0.37	73.0	0.6	1.7	0.5	1.7	3.8
	<b>387.5</b>	26	58.5	0.34	74.9	0.7	1.8	0.4	1.8	4.1
	<b>412.5</b>	28	56.3	0.34	76.9	0.8	2.0	0.5	2.0	4.3
	<b>437.5</b>	30	53.0	0.28	77.4	1.0	2.1	0.3	2.1	4.5
	<b>462.5</b>	32	51.1	0.29	79.6	1.1	2.2	0.4	2.2	4.8
	<b>487.5</b>	34	49.6	0.29	82.1	1.2	2.4	0.6	2.4	5.0
	<b>512.5</b>	36	47.5	0.28	83.2	1.3	2.5	0.6	2.5	5.2
	<b>537.5</b>	38	45.8	0.27	84.7	1.4	2.7	0.6	2.7	5.4
	<b>562.5</b>	40	43.9	0.24	85.5	1.6	2.8	0.5	2.8	5.6
	<b>587.5</b>	43	41.7	0.24	87.1	1.7	3.0	0.5	3.0	5.8
<b>0.07</b>	<b>337.5</b>	21	62.2	0.37	72.8	0.6	1.7	0.4	1.7	3.8
	<b>362.5</b>	22	58.7	0.34	74.5	0.7	1.8	0.4	1.8	4.1
	<b>387.5</b>	24	56.4	0.34	77.4	0.8	2.0	0.6	2.0	4.3
	<b>412.5</b>	26	53.4	0.31	78.1	1.0	2.1	0.5	2.1	4.5
	<b>437.5</b>	28	50.8	0.28	79.5	1.1	2.3	0.4	2.3	4.8
	<b>462.5</b>	29	48.6	0.26	81.1	1.2	2.4	0.4	2.4	5.0
	<b>487.5</b>	31	46.7	0.26	82.8	1.3	2.6	0.5	2.6	5.2
	<b>512.5</b>	33	45.1	0.25	84.6	1.5	2.7	0.6	2.7	5.4
	<b>537.5</b>	35	43.6	0.25	86.4	1.6	2.9	0.6	2.9	5.7
	<b>562.5</b>	37	41.7	0.24	87.1	1.7	3.0	0.5	3.0	5.9
	<b>587.5</b>	39	40.6	0.25	89.0	1.9	3.2	0.7	3.2	6.0
		<b>600.0</b>	40	39.9	0.26	89.4	1.9	3.2	0.7	3.3

<sup>1</sup>values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $Du_{lq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

<b>Table 4c</b> Lookup table for basins with a bed slope of 0.1%, <i>CITRUS</i>										
$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	-	<i>min</i>	%	%	%	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.08</b>	<b>337.5</b>	19	59.8	0.36	74.3	0.7	1.8	0.5	1.8	4.0
	<b>362.5</b>	21	56.3	0.33	75.8	0.8	1.9	0.5	1.9	4.3
	<b>387.5</b>	22	53.4	0.30	77.7	0.9	2.1	0.5	2.1	4.5
	<b>412.5</b>	24	51.0	0.28	79.2	1.1	2.2	0.4	2.2	4.8
	<b>437.5</b>	26	48.7	0.26	80.9	1.2	2.4	0.3	2.4	5.0
	<b>462.5</b>	27	46.7	0.26	82.8	1.3	2.6	0.5	2.6	5.2
	<b>487.5</b>	29	44.6	0.24	84.0	1.5	2.7	0.4	2.7	5.5
	<b>512.5</b>	31	42.9	0.23	85.5	1.6	2.9	0.4	2.9	5.7
	<b>537.5</b>	32	41.8	0.25	88.1	1.8	3.1	0.6	3.1	5.9
	<b>562.5</b>	34	40.1	0.25	89.0	1.9	3.2	0.6	3.2	6.1
	<b>587.5</b>	36	38.7	0.26	90.2	2.1	3.4	0.5	3.4	6.3
<b>600.0</b>	37	38.3	0.27	91.2	2.1	3.5	0.6	3.5	6.4	
<b>0.09</b>	<b>337.5</b>	18	56.7	0.30	74.2	0.8	1.9	0.2	1.9	4.2
	<b>362.5</b>	19	54.2	0.30	77.0	0.9	2.0	0.4	2.0	4.5
	<b>387.5</b>	21	51.2	0.28	78.6	1.0	2.2	0.4	2.2	4.7
	<b>412.5</b>	22	49.3	0.28	80.7	1.2	2.4	0.5	2.4	5.0
	<b>437.5</b>	24	46.8	0.25	82.0	1.3	2.5	0.5	2.5	5.2
	<b>462.5</b>	26	44.8	0.23	83.8	1.5	2.7	0.4	2.7	5.5
	<b>487.5</b>	27	43.2	0.24	85.9	1.6	2.9	0.6	2.9	5.7
	<b>512.5</b>	29	41.8	0.25	88.0	1.8	3.1	0.6	3.1	5.9
	<b>537.5</b>	30	39.8	0.24	88.5	1.9	3.2	0.4	3.2	6.1
	<b>562.5</b>	32	38.7	0.27	90.6	2.1	3.4	0.6	3.4	6.3
	<b>587.5</b>	34	37.5	0.28	92.3	2.2	3.6	0.6	3.6	6.5
<b>600.0</b>	34	36.9	0.29	92.7	2.3	3.7	0.6	3.7	6.6	

<sup>1</sup>values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $Du_{lq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

Table 4d Lookup table for basins with a bed slope of 0.1%, CITRUS										
$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
cfs/ft	-	min	%	%	%	in	in	in	in	In
0.10	337.5	17	56.1	0.33	77.0	0.9	2.0	0.6	2.0	4.3
	362.5	18	52.6	0.30	78.3	1.0	2.1	0.5	2.1	4.6
	387.5	20	49.6	0.27	79.8	1.1	2.3	0.5	2.3	4.9
	412.5	21	47.4	0.25	81.4	1.3	2.5	0.4	2.5	5.1
	437.5	23	45.3	0.23	83.3	1.4	2.7	0.4	2.7	5.4
	462.5	24	43.9	0.25	86.1	1.6	2.9	0.6	2.8	5.6
	487.5	26	41.5	0.23	86.4	1.7	3.0	0.5	3.0	5.9
	512.5	27	40.2	0.25	88.8	1.9	3.2	0.6	3.2	6.1
	537.5	29	38.8	0.26	90.5	2.1	3.4	0.6	3.4	6.3
	562.5	30	37.4	0.28	92.0	2.2	3.6	0.6	3.6	6.6
	587.5	32	36.1	0.30	93.3	2.4	3.8	0.6	3.8	6.8
600.0	32	35.5	0.31	93.7	2.5	3.8	0.4	3.8	6.8	
0.11	337.5	16	53.5	0.29	76.6	0.9	2.1	0.3	2.1	4.5
	362.5	17	51.6	0.29	79.5	1.1	2.2	0.6	2.2	4.7
	387.5	19	48.3	0.26	80.6	1.2	2.4	0.4	2.4	5.0
	412.5	20	45.8	0.24	82.4	1.4	2.6	0.4	2.6	5.3
	437.5	22	43.7	0.22	74.1	1.5	2.8	0.3	2.8	5.6
	462.5	23	42.4	0.24	87.2	1.7	3.0	0.6	3.0	5.8
	487.5	24	40.1	0.23	87.7	1.9	3.2	0.4	3.2	6.1
	512.5	26	39.0	0.25	89.7	2.0	3.3	0.5	3.3	6.3
	537.5	27	37.7	0.28	91.7	2.2	3.6	0.6	3.5	6.5
	562.5	29	36.2	0.30	92.9	2.4	3.7	0.6	3.7	6.7
	587.5	30	35.1	0.33	94.7	2.5	3.9	0.6	3.9	7.0
600.0	31	34.6	0.34	95.4	2.6	4.0	0.6	4.0	7.0	

<sup>1</sup>values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $Du_{lq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
cfs/ft	-	min	%	%	%	in	in	in	in	in
<b>0.12</b>	<b>337.5</b>	15	52.2	0.29	77.7	1.0	2.1	0.4	2.1	4.6
	<b>362.5</b>	16	49.4	0.26	79.1	1.1	2.3	0.4	2.3	4.9
	<b>387.5</b>	18	46.8	0.24	81.3	1.3	2.5	0.3	2.5	5.2
	<b>412.5</b>	19	44.8	0.24	83.8	1.5	2.7	0.5	2.7	5.5
	<b>437.5</b>	21	42.5	0.22	85.2	1.6	2.9	0.4	2.9	5.7
	<b>462.5</b>	22	40.6	0.23	86.9	1.8	3.1	0.3	3.1	6.0
	<b>487.5</b>	23	38.9	0.24	88.5	2.0	3.3	0.2	3.3	6.2
	<b>512.5</b>	25	37.7	0.26	90.3	2.1	3.5	0.4	3.5	6.4
	<b>537.5</b>	26	36.6	0.29	92.7	2.3	3.7	0.6	3.7	6.7
	<b>562.5</b>	27	35.3	0.32	94.4	2.5	3.9	0.6	3.9	6.9
	<b>587.5</b>	29	34.1	0.35	95.8	2.7	4.1	0.6	4.1	7.1
<b>600.0</b>	30	33.7	0.36	96.8	2.8	4.2	0.6	4.2	7.2	
<b>0.13</b>	<b>312.5</b>	13	53.9	0.29	75.9	0.9	2.0	0.3	2.0	4.6
	<b>337.5</b>	15	51.5	0.29	79.5	1.1	2.2	0.6	2.2	4.8
	<b>362.5</b>	16	48.5	0.26	80.6	1.2	2.4	0.4	2.4	5.0
	<b>387.5</b>	17	45.7	0.23	82.3	1.4	2.6	0.4	2.6	5.3
	<b>412.5</b>	18	43.4	0.22	84.2	1.6	2.8	0.3	2.8	5.6
	<b>437.5</b>	20	41.4	0.22	86.0	1.7	3.0	0.3	3.0	5.9
	<b>462.5</b>	21	39.7	0.24	88.2	1.9	3.2	0.4	3.2	6.1
	<b>487.5</b>	22	38.3	0.26	90.5	2.1	3.4	0.6	2.1	6.4
	<b>512.5</b>	24	37.1	0.29	92.2	2.3	3.6	0.6	3.6	6.6
	<b>537.5</b>	25	35.6	0.31	93.6	2.4	3.8	0.4	3.8	6.9
	<b>562.5</b>	26	34.4	0.34	95.4	2.6	4.0	0.6	4.0	7.1
<b>587.5</b>	28	33.3	0.37	97.1	2.8	4.3	0.7	4.3	7.3	
<b>600.0</b>	29	32.8	0.38	97.8	2.9	4.3	0.8	4.3	7.4	

<sup>1</sup>values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $Du_{lq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

<b>Table 4f</b> Lookup table for basins with a bed slope of 0.1%, <i>CITRUS</i>										
$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	-	<i>min</i>	%	%	%	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.14</b>	<b>337.5</b>	14	49.6	0.26	79.2	1.1	2.3	0.3	2.3	4.9
	<b>362.5</b>	15	47.0	0.23	80.8	1.3	2.5	0.3	2.5	5.2
	<b>387.5</b>	16	44.9	0.23	83.6	1.5	2.7	0.5	2.7	5.5
	<b>412.5</b>	18	42.4	0.22	85.2	1.6	2.9	0.4	2.9	5.7
	<b>437.5</b>	19	40.4	0.23	86.9	1.8	3.1	0.3	3.1	6.0
	<b>462.5</b>	20	38.9	0.25	89.3	2.0	3.3	0.5	3.3	6.3
	<b>487.5</b>	21	37.5	0.28	91.7	2.2	3.6	0.6	3.6	6.5
	<b>512.5</b>	23	36.2	0.30	93.1	2.4	3.7	0.6	3.7	6.8
	<b>537.5</b>	24	34.9	0.33	95.0	2.6	4.0	0.6	4.0	7.0
	<b>562.5</b>	25	33.6	0.36	96.5	2.8	4.2	0.6	4.2	7.2
	<b>587.5</b>	27	32.5	0.39	98.1	3.0	4.4	0.8	4.4	7.5
	<b>600.0</b>	28	31.9	0.41	98.4	3.0	4.5	0.9	4.5	7.6
<b>0.15</b>	<b>337.5</b>	14	48.5	0.25	79.8	1.2	2.4	0.4	2.4	5.0
	<b>362.5</b>	15	46.1	0.23	81.7	1.4	2.6	0.4	2.6	5.3
	<b>387.5</b>	16	43.6	0.22	83.8	1.5	2.8	0.3	2.8	5.6
	<b>412.5</b>	17	41.4	0.22	85.8	1.7	3.0	0.2	3.0	5.9
	<b>437.5</b>	18	39.7	0.24	88.2	1.9	3.2	0.4	3.2	6.2
	<b>462.5</b>	19	37.8	0.25	89.7	2.1	3.4	0.3	3.5	6.4
	<b>487.5</b>	21	36.6	0.29	92.4	2.3	3.7	0.5	3.7	6.7
	<b>512.5</b>	22	35.5	0.32	94.3	2.5	3.9	0.6	3.9	6.9
	<b>537.5</b>	23	34.1	0.35	95.9	2.7	4.1	0.6	4.1	7.2
	<b>562.5</b>	24	32.9	0.38	97.6	2.9	4.3	0.8	4.3	7.4
	<b>587.5</b>	26	31.7	0.41	98.9	3.1	4.6	1.0	4.6	7.6
	<b>600.0</b>	27	31.1	0.42	99.1	3.2	4.7	1.1	4.7	7.7

<sup>1</sup>values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $Du_{lq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

<b>Table 4g</b> Lookup table for basins with a bed slope of 0.1%, <i>CITRUS</i>										
$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	-	<i>min</i>	%	%	%	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.16</b>	<b>337.5</b>	13.04	48.1	0.26	81.6	1.3	2.5	0.6	2.5	5.1
	<b>362.5</b>	14.04	45.3	0.23	82.7	1.4	2.6	0.4	2.6	5.4
	<b>387.5</b>	15.22	42.8	0.22	84.7	1.6	2.9	0.4	2.9	5.7
	<b>412.5</b>	16.41	40.6	0.22	86.7	1.8	3.1	0.3	3.1	6.0
	<b>437.5</b>	17.58	38.7	0.24	88.5	2.0	3.3	0.2	3.3	6.3
	<b>462.5</b>	18.80	37.5	0.28	91.7	2.2	3.6	0.6	3.6	6.6
	<b>487.5</b>	20.00	35.8	0.30	93.1	2.4	3.8	0.3	3.8	6.8
	<b>512.5</b>	21.03	34.8	0.33	95.2	2.6	4.0	0.6	4.0	7.0
	<b>537.5</b>	22.26	33.5	0.37	97.0	2.8	4.2	0.7	4.2	7.3
	<b>562.5</b>	23.50	32.2	0.40	98.4	3.0	4.5	0.9	4.5	7.5
	<b>587.5</b>	24.71	30.9	0.43	99.3	3.2	4.7	1.1	4.7	7.8
<b>600.0</b>	25.25	30.3	0.44	99.5	3.3	4.8	1.2	4.8	7.9	
<b>0.17</b>	<b>337.5</b>	12.61	46.5	0.23	81.0	1.3	2.5	0.3	2.5	5.3
	<b>362.5</b>	13.58	44.9	0.24	84.3	1.5	2.7	0.6	2.7	5.5
	<b>387.5</b>	14.73	42.1	0.22	85.7	1.7	3.0	0.4	3.0	5.8
	<b>412.5</b>	15.88	39.9	0.23	87.6	1.9	3.2	0.4	3.2	6.1
	<b>437.5</b>	17.01	38.0	0.25	89.3	2.1	3.4	0.3	3.4	6.4
	<b>462.5</b>	18.18	36.6	0.28	92.0	2.3	3.7	0.2	3.7	6.7
	<b>487.5</b>	19.36	35.3	0.32	94.5	2.5	3.9	0.6	3.9	6.9
	<b>512.5</b>	20.36	34.1	0.35	96.0	2.7	4.1	0.6	4.1	7.2
	<b>537.5</b>	21.56	32.8	0.38	97.7	2.9	4.3	0.8	4.3	7.4
	<b>562.5</b>	22.76	31.5	0.42	99.1	3.1	4.6	1.0	4.6	7.7
	<b>587.5</b>	23.93	30.1	0.44	99.6	3.4	4.8	1.2	4.8	7.9
<b>600.0</b>	24.45	29.5	0.46	99.7	3.5	4.9	1.4	4.9	8.0	

<sup>1</sup>values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $Du_{lq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

<b>Table 4h</b> Lookup table for basins with a bed slope of 0.1%, <i>CITRUS</i>										
$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	-	<i>min</i>	%	%	%	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.18</b>	<b>337.5</b>	12	45.8	0.23	82.0	1.4	2.6	0.4	2.6	5.5
	<b>362.5</b>	13	43.5	0.22	83.8	1.6	2.8	0.3	2.8	5.6
	<b>387.5</b>	14	41.1	0.21	85.9	1.8	3.0	0.3	3.0	5.9
	<b>412.5</b>	15	39.7	0.25	89.5	2.0	3.3	0.6	3.3	6.2
	<b>437.5</b>	17	37.5	0.26	90.5	2.2	3.5	0.4	3.5	6.5
	<b>462.5</b>	18	36.0	0.30	92.9	2.4	3.8	0.3	3.8	6.8
	<b>487.5</b>	19	34.7	0.33	95.4	2.6	4.0	0.6	4.0	7.1
	<b>512.5</b>	20	33.5	0.37	96.9	2.8	4.2	0.7	4.2	7.3
	<b>537.5</b>	21	32.1	0.40	98.2	3.0	4.5	0.9	4.5	7.6
	<b>562.5</b>	22	30.8	0.43	99.5	3.3	4.7	1.1	4.7	7.8
	<b>587.5</b>	23	29.4	0.46	99.9	3.5	5.0	1.4	5.0	8.1
	<b>600.0</b>	24	28.8	0.47	100.0	3.6	5.1	1.5	5.1	8.2
<b>0.19</b>	<b>337.5</b>	12	45.2	0.23	82.9	1.4	2.7	0.4	2.7	5.7
	<b>362.5</b>	13	42.8	0.22	84.6	1.6	2.9	0.4	2.9	5.7
	<b>387.5</b>	14	40.4	0.22	86.6	1.8	3.1	0.3	3.1	6.0
	<b>412.5</b>	15	38.4	0.24	88.7	2.0	3.4	0.3	3.4	6.3
	<b>437.5</b>	16	37.0	0.28	91.6	2.2	3.6	0.5	3.6	6.6
	<b>462.5</b>	17	35.5	0.31	93.9	2.5	3.9	0.6	3.9	6.9
	<b>487.5</b>	18	34.1	0.35	96.1	2.7	4.1	0.6	4.1	7.2
	<b>512.5</b>	19	32.9	0.38	97.6	2.9	4.3	0.8	4.3	7.4
	<b>537.5</b>	20	31.5	0.41	98.8	3.1	4.6	1.0	4.6	7.7
	<b>562.5</b>	21	30.0	0.45	99.4	3.4	4.8	1.3	4.8	7.9
	<b>587.5</b>	23	28.6	0.47	99.7	3.6	5.1	1.5	5.1	8.2
	<b>600.0</b>	24	28.0	0.48	99.7	3.7	5.2	1.6	5.2	8.3

<sup>1</sup>values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $Du_{lq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

<b>Table 4i</b> Lookup table for basins with a bed slope of 0.1%, <i>CITRUS</i>										
$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
cfs/ft	-	Min	%	%	%	in	in	in	in	in
<b>0.21</b>	<b>337.5</b>	12	44.8	0.24	84.1	1.5	2.7	0.6	2.7	5.8
	<b>362.5</b>	13	42.2	0.22	85.4	1.7	2.9	0.4	2.9	5.9
	<b>387.5</b>	14	40.0	0.23	87.7	1.9	3.2	0.4	3.2	6.1
	<b>412.5</b>	15	37.9	0.25	89.7	2.1	3.4	0.3	3.4	6.4
	<b>437.5</b>	16	36.3	0.29	92.1	2.3	3.7	0.3	3.7	6.7
	<b>462.5</b>	17	35.0	0.33	94.8	2.5	3.9	0.5	3.9	7.0
	<b>487.5</b>	18	33.5	0.36	96.7	2.8	4.2	0.6	4.2	7.3
	<b>512.5</b>	19	32.3	0.40	98.1	3.0	4.4	0.9	4.4	7.5
	<b>537.5</b>	20	30.9	0.43	99.4	3.2	4.7	1.1	4.7	7.8
	<b>562.5</b>	21	29.4	0.46	99.8	3.5	5.0	1.4	5.0	8.1
	<b>587.5</b>	22	28.0	0.48	100.0	3.7	5.2	1.6	5.2	8.3
	<b>600.0</b>	23	27.4	0.50	100.0	3.9	5.3	1.7	5.3	8.5
<b>0.22</b>	<b>337.5</b>	11	43.6	0.21	83.7	1.5	2.8	0.3	2.8	6.0
	<b>362.5</b>	12	41.3	0.21	85.4	1.7	3.0	0.2	3.0	6.0
	<b>387.5</b>	13	39.7	0.25	89.1	2.0	3.3	0.5	3.3	6.2
	<b>412.5</b>	14	37.4	0.26	90.5	2.2	3.5	0.4	3.5	6.5
	<b>437.5</b>	15	35.8	0.30	92.8	2.4	3.8	0.3	3.8	6.8
	<b>462.5</b>	16	34.4	0.34	95.4	2.6	4.0	0.5	4.0	7.1
	<b>487.5</b>	17	33.0	0.38	97.5	2.9	4.3	0.7	4.3	7.4
	<b>512.5</b>	18	31.8	0.41	98.8	3.1	4.5	1.0	4.5	7.6
	<b>537.5</b>	19	30.2	0.44	99.3	3.3	4.8	1.2	4.8	7.9
	<b>562.5</b>	20	28.7	0.47	99.7	3.6	5.1	1.5	5.1	8.2
	<b>587.5</b>	21	27.3	0.50	99.7	3.9	5.3	1.8	5.3	8.5
	<b>600.0</b>	22	26.7	0.51	99.7	4.0	5.5	1.9	5.5	8.6

<sup>1</sup>values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $Du_{lq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

<b>Table 4j</b> Lookup table for basins with a bed slope of 0.1%, <i>CITRUS</i>										
$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$
<i>cfs/ft</i>	<i>ft</i>	<i>Min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>
<b>0.22</b>	<b>337.5</b>	11	43.0	0.21	84.3	1.6	2.8	0.3	2.8	6.1
	<b>362.5</b>	12	40.8	0.22	86.2	1.8	3.1	0.3	3.1	6.2
	<b>387.5</b>	13	38.6	0.23	88.4	2.0	3.3	0.2	3.3	6.3
	<b>412.5</b>	14	37.2	0.28	92.0	2.3	3.6	0.3	3.6	6.6
	<b>437.5</b>	15	35.5	0.32	94.1	2.5	3.9	0.6	3.9	6.9
	<b>462.5</b>	16	33.9	0.35	96.0	2.7	4.1	0.6	4.1	7.2
	<b>487.5</b>	17	32.5	0.39	98.0	3.0	4.4	0.8	4.4	7.5
	<b>512.5</b>	18	31.2	0.42	99.1	3.2	4.6	1.1	4.6	7.7
	<b>537.5</b>	19	29.6	0.45	99.5	3.4	4.9	1.3	4.9	8.0
	<b>562.5</b>	20	28.1	0.48	99.8	3.7	5.2	1.6	5.2	8.3
	<b>587.5</b>	21	26.7	0.51	99.8	4.0	5.5	1.9	5.5	8.6
<b>600.0</b>	22	26.2	0.52	100.0	4.1	5.6	2.0	5.6	8.7	
<b>0.23</b>	<b>337.5</b>	11	42.5	0.22	85.0	1.6	2.9	0.4	2.9	6.3
	<b>362.5</b>	12	40.3	0.22	86.9	1.8	3.1	0.3	3.1	6.3
	<b>387.5</b>	13	38.1	0.24	89.1	2.1	3.4	0.3	3.4	6.4
	<b>412.5</b>	14	36.5	0.28	92.1	2.3	3.7	0.2	3.7	6.7
	<b>437.5</b>	15	35.0	0.33	94.7	2.5	3.9	0.5	3.9	7.0
	<b>462.5</b>	16	33.5	0.37	96.9	2.8	4.2	0.7	4.2	7.3
	<b>487.5</b>	17	32.0	0.40	98.6	3.0	4.5	0.9	4.5	7.6
	<b>512.5</b>	18	30.6	0.43	99.2	3.3	4.7	1.2	4.7	7.9
	<b>537.5</b>	19	29.1	0.46	99.9	3.5	5.0	1.4	5.0	8.1
	<b>562.5</b>	20	27.5	0.49	99.7	3.8	5.3	1.7	5.3	8.4
	<b>587.5</b>	21	26.2	0.52	99.9	4.1	5.6	2.0	5.6	8.7
<b>600.0</b>	22	25.6	0.53	99.9	4.2	5.7	2.1	5.7	8.8	

<sup>1</sup>values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $Du_{lq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

<b>Table 4k</b> Lookup table for basins with a bed slope of 0.1%, <i>CITRUS</i>											
$q_o$	$L_{co}$	$t_{co}^1$	$E_a$	$Du_{lq}$	$E_r$	$D_p$	$D_{av}$	$D_{min}$	$D_{app}$	$Y_{max}$	
<i>cfs/ft</i>	<i>ft</i>	<i>Min</i>	<i>%</i>	<i>%</i>	<i>%</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	<i>in</i>	
<b>0.24</b>	<b>337.5</b>	10	42.3	0.23	86.3	1.7	3.0	0.5	3.0	6.4	
	<b>362.5</b>	11	39.9	0.23	87.7	1.9	3.2	0.4	3.2	6.5	
	<b>387.5</b>	12	37.7	0.26	90.0	2.1	3.5	0.3	3.5	6.5	
	<b>412.5</b>	13	35.9	0.29	92.4	2.4	3.7	0.3	3.7	6.8	
	<b>437.5</b>	14	34.5	0.34	95.2	2.6	4.0	0.5	4.0	7.1	
	<b>462.5</b>	15	33.0	0.38	97.4	2.9	4.3	0.7	4.3	7.4	
	<b>487.5</b>	16	31.5	0.42	99.0	3.1	4.6	1.0	4.6	7.7	
	<b>512.5</b>	17	30.1	0.44	99.6	3.4	4.8	1.2	4.8	8.0	
	<b>537.5</b>	18	28.5	0.47	99.8	3.6	5.1	1.5	5.1	8.2	
	<b>562.5</b>	19	27.0	0.50	99.9	3.9	5.4	1.8	5.4	8.5	
	<b>600.0</b>	20	2.5	0.54	100.0	4.3	5.8	2.2	5.8	9.0	
<b>0.25</b>	<b>337.5</b>	10	41.2	0.21	85.7	1.8	3.0	0.2	3.0	6.6	
	<b>362.5</b>	11	39.7	0.24	88.9	2.0	3.3	0.5	3.3	6.6	
	<b>387.5</b>	12	37.3	0.26	90.7	2.2	3.5	0.4	3.5	6.7	
	<b>412.5</b>	13	35.6	0.30	93.3	2.4	3.8	0.3	3.8	6.9	
	<b>437.5</b>	14	34.1	0.35	95.9	2.7	4.1	0.5	4.1	7.2	
	<b>462.5</b>	15	32.6	0.39	98.0	2.9	4.4	0.8	4.4	7.5	
	<b>487.5</b>	16	31.0	0.43	99.2	3.2	4.7	1.1	4.7	7.8	
	<b>512.5</b>	17	29.6	0.45	99.8	3.5	4.9	1.3	4.9	8.1	
	<b>537.5</b>	18	28.0	0.48	99.9	3.7	5.2	1.6	5.2	8.4	
	<b>562.5</b>	19	26.5	0.51	99.9	4.0	5.5	1.9	5.5	8.7	
		<b>587.5</b>	20	25.2	0.54	99.9	4.3	5.8	2.2	5.8	8.9
		<b>600.0</b>	21	24.6	0.55	99.9	4.5	5.9	2.3	5.9	9.1

<sup>1</sup>values are rounded-off to the nearest integer,  $q_o$  = unit inlet flow rate,  $L_{co}$  = cutoff distance,  $t_{co}$  = cutoff time,  $E_a$  = application efficiency,  $Du_{lq}$  = low quarter distribution efficiency,  $E_r$  = water requirement efficiency,  $D_p$  = deep percolation depth,  $D_{av}$  = average depth,  $D_{min}$  = minimum depth,  $Y_{max}$  = maximum flow depth (the total depth of the border ridge can be calculated as the sum of  $Y_{max}$  and a 50% to 100% allowance for freeboard).

Table 5. Coefficients and exponents of the power-law advance function

Unit inlet flow rate (cfs/s)	Citrus basins				Alfalfa basins	
	Level basin		0.1% slope		Level basin	
	$\alpha$ (min/ft $^\beta$ )*	$\beta$ (-)*	$\alpha$ (min/ft $^\beta$ )*	$\beta$ (-)*	$\alpha$ (min/ft $^\beta$ )*	$\beta$ (-)*
0.04	0.0231	1.2502	0.0382	1.1339	0.034285	1.2467
0.05	0.0204	1.2474	0.0318	1.1429	0.029765	1.2474
0.06	0.0183	1.2465	0.0143	1.2465	0.024541	1.2606
0.07	0.0217	1.2045	0.0251	1.1509	0.024814	1.2443
0.08	0.0155	1.2448	0.0222	1.1594	0.023367	1.2406
0.09	0.0144	1.2449	0.0204	1.1625	0.019324	1.2596
0.10	0.0133	1.2474	0.0204	1.1537	0.020706	1.2393
0.11	0.0126	1.2472	0.0178	1.1672	0.019679	1.2379
0.12	0.0119	1.2472	0.0163	1.1739	0.01535	1.2699
0.13	0.0114	1.2470	0.0154	1.1761	0.016862	1.2476
0.14	0.0107	1.2505	0.0146	1.1778	0.015725	1.2518
0.15	0.0101	1.2532	0.0139	1.1798	0.01374	1.2674
0.16	0.0099	1.2503	0.0133	1.1809	0.012095	1.2819
0.17	0.0095	1.2501	0.0128	1.1826	0.014565	1.2469
0.18	0.0092	1.2504	0.0123	1.1836	0.014585	1.2424
0.19	0.0089	1.2500	0.0118	1.1854	0.011839	1.2699
0.20	0.0088	1.2475	0.0110	1.1925	0.010673	1.282
0.21	0.0086	1.2466	0.0107	1.1934	0.012073	1.2569
0.22	0.0084	1.2468	0.0104	1.1944	0.010571	1.2749
0.23	0.0081	1.2474	0.0100	1.1960	0.010359	1.2743
0.24	0.0079	1.2476	0.0099	1.1942	0.010597	1.2654
0.25	0.0078	1.2470	0.0095	1.1968	0.013354	1.2254

\*  $\alpha$  and  $\beta$  are parameters of the power-law advance function:  $t_{co} = t_a = \alpha L_{co}^\beta$

